

# HA17301P

## Quad Operational Amplifier

# HITACHI

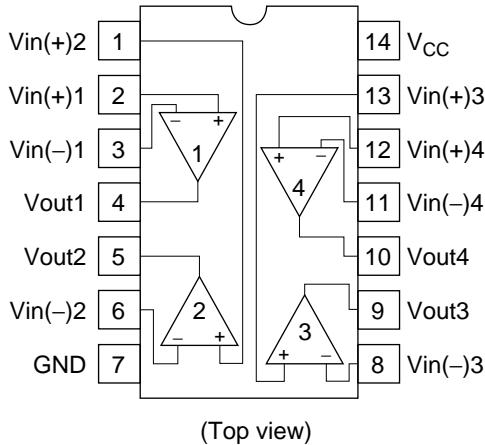
### Description

The HA17301P is an internal-compensation quad operational amplifier that operates on a single-voltage power supply. Typical applications for the HA17301P include waveform generators, voltage regulators, logic circuits, and voltage-controlled oscillators.

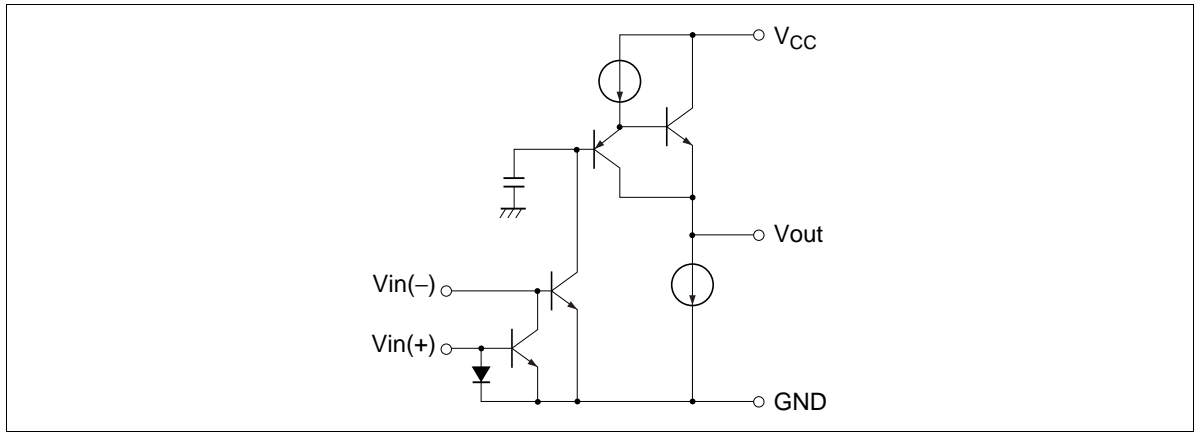
### Features

- Wide operating temperature range
- Single-voltage power supply operation
- Internal phase compensation
- Low input bias current

### Pin Arrangement



**Circuit Structure (1/4)**



**Absolute Maximum Ratings** ( $T_a = 25^\circ\text{C}$ )

| Item                         | Symbol       | Ratings     | Unit             |
|------------------------------|--------------|-------------|------------------|
| Power-supply voltage         | $V_{CC}$     | 28          | V                |
| Noninverting input current   | $I_r$        | 5           | mA               |
| Sink current                 | $I_o$ sink   | 50          | mA               |
| Source current               | $I_o$ source | 50          | mA               |
| Allowable power dissipation* | $P_T$        | 625         | mW               |
| Operating temperature        | $T_{opr}$    | -20 to +75  | $^\circ\text{C}$ |
| Storage temperature          | $T_{stg}$    | -55 to +125 | $^\circ\text{C}$ |

Note: This is the allowable value up to  $T_a = 50^\circ\text{C}$  for the HA17301P. Derate by 8.3 mW/ $^\circ\text{C}$  above that temperature.

**Electrical Characteristics** ( $V_{CC} = +15\text{ V}$ ,  $R_L = 5.0\text{ k}\Omega$ ,  $T_a = 25^\circ\text{C}$ )

| Item                         | Symbol        | Min   | Typ   | Max  | Unit             | Test Conditions                                    |
|------------------------------|---------------|-------|-------|------|------------------|--|
| Voltage gain                 | $A_{VD}$      | 1,000 | 1,400 | —    | V/V              |  |
| Supply current               | $I_{CO}$      | —     | 7.7   | 10   | mA               | Non inverting input open                           |
|                              | $I_{CG}$      | —     | 8.3   | 14   | mA               | Non inverting input grounded                       |
| Input bias current           | $I_{IB}$      | —     | 80    | 300  | nA               | $R_L = \infty$                                     |
| Current mirror gain          | $A_I$         | 0.80  | 0.94  | 1.16 | A/A              | $I_r = 200\ \mu\text{A}$                           |
| Output source current        | $I_o$ source  | 3     | 13    | —    | mA               | $V_{OH} = 0.4\text{ V}$                            |
|                              |               | —     | 10    | —    | mA               | $V_{OH} = 9.0\text{ V}$                            |
| Output sink current          | $I_o$ sink    | 0.5   | 0.75  | —    | mA               | $V_{OL} = 0.4\text{ V}$                            |
| Output voltage               | $V_{OH}$      | 13.5  | 13.9  | —    | V                |  |
|                              | $V_{OL(inv)}$ | —     | 0.04  | 0.1  | V                | Inverting input driven                             |
|                              | $V_{OL(non)}$ | —     | 0.55  | —    | V                | Non inverting input driven                         |
| Input resistance             | $R_{in}$      | 0.1   | 1.0   | —    | $\text{M}\Omega$ | Inverting input only                               |
| Slew rate                    | SR            | —     | 0.2   | —    | V/ $\mu\text{s}$ | $C_L = 100\text{ pF}$ , $R_L = 5.0\text{ k}\Omega$ |
| Bandwidth                    | BW            | —     | 2.6   | —    | MHz              | $A_{VD} = 1$                                       |
| Phase margin                 | $\phi_m$      | —     | 87    | —    | deg              |  |
| Power-supply rejection ratio | PSRR          | —     | 63    | —    | dB               | $f = 100\text{ Hz}$                                |
| Channel separation           | CS            | —     | 63    | —    | dB               | $f = 1.0\text{ kHz}$                               |

## HA17301P Application Examples

The HA17301P is a quad operational amplifier, and consists of four operational amplifier circuits and one bias current circuit. The HA17301P features a wide operating temperature range, single-voltage power supply operation, internal phase compensation, a wide zero-cross bandwidth, a low input bias current, and a high open-loop gain. Thus the HA17301P can be used in a wide range of applications. This section describes several applications using the HA17301P.

### HA17301 Circuit Operation

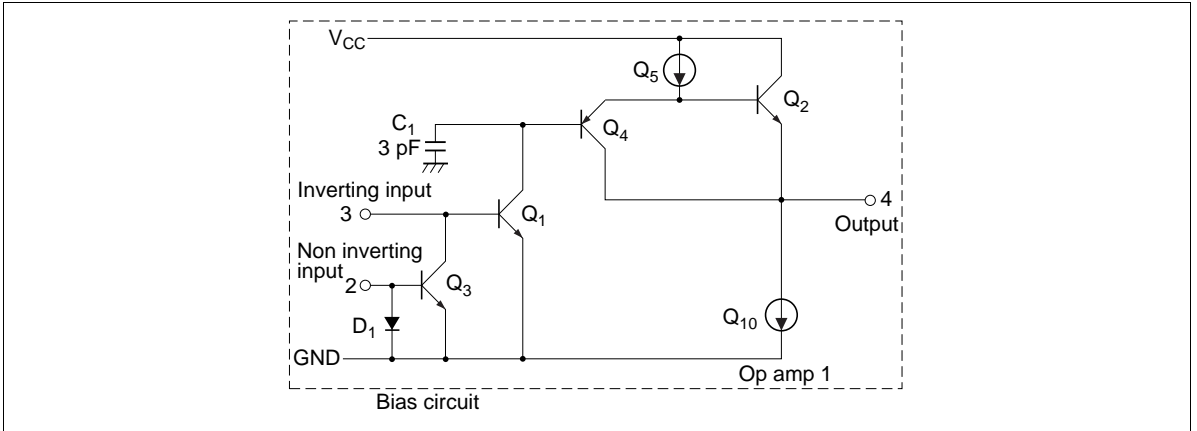


Figure 1 HA17301 Internal Equivalent Circuit

Figure 1 shows the internal equivalent circuit for the HA17301P bias circuit and one operational amplifier circuit (Op amp 1).

Op amp 1 is basically an emitter ground type operational amplifier in which the input transistor  $Q_1$ , the buffer transistor  $Q_4$ , the current source transistor  $Q_5$ , the output emitter-follower transistor  $Q_2$ , and the current source transistor  $Q_{10}$  form an inverting amplifier. The voltage gain of this circuit is all given by the transistor  $Q_1$ , and the adoption of the current-supply load  $Q_3$  allows this circuit to provide a large open-loop gain even at low power-supply voltages. Next, the emitter-follower transistor  $Q_2$  lowers the output impedance of this circuit. The use of the power-supply transistor  $Q_{10}$  as the load for  $Q_2$  gives this circuit an extremely large dynamic range, and essentially an amplitude from ground to  $(V_{CC} - 1)$  can be acquired. Also, the buffer transistor  $Q_4$  is used to reduce the input current without increasing the DC input voltage level. Since the capacitor  $C_1$  is used to preserve stability when this inverting amplifier is used as a closed circuit, no external compensation is required.

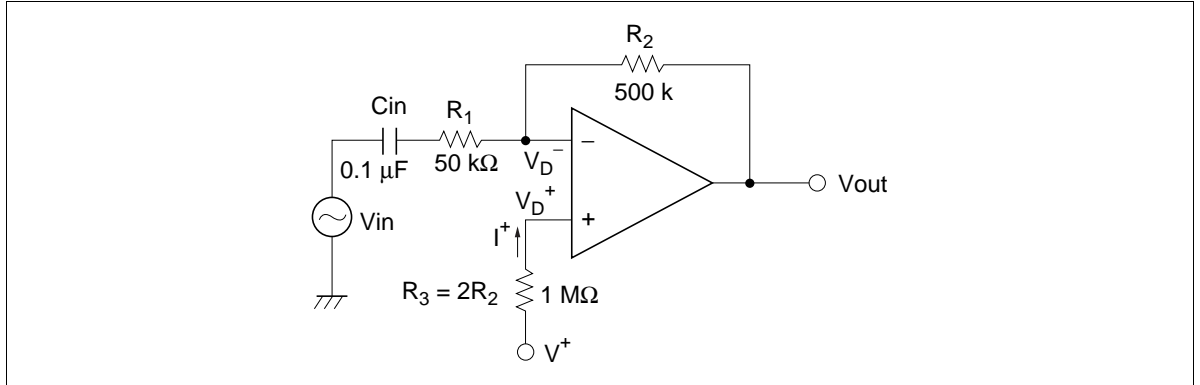
Now consider the non inverting circuit. Assuming that the current amplification ratio provided by  $Q_3$  is adequately large for the current flowing into the non inverting input, then all that current will flow through diode  $D_1$  and the voltage drop induced in the diode  $D_1$  by this input current will be applied to the  $Q_3$  base-emitter junction. Therefore, if  $D_1$  and  $Q_3$  are matched, a current equal to the input current will flow in the  $Q_3$  emitter. Assuming that the current amplification ratio provided by  $Q_3$  is adequately large, a current equal to the input current will flow in the  $Q_3$  collector. This is called a “current mirror”, and when an external feedback resistor is used, a current equal to the non inverting input current will flow in this resistor and thus determine the output voltage.

## Inverting Amplifier

There are three bias techniques for biasing the inverting amplifier, the single power supply bias technique, the  $NV_{BE}$  bias technique, and the load voltage bias technique.

### 1. Single Power Supply Bias Technique

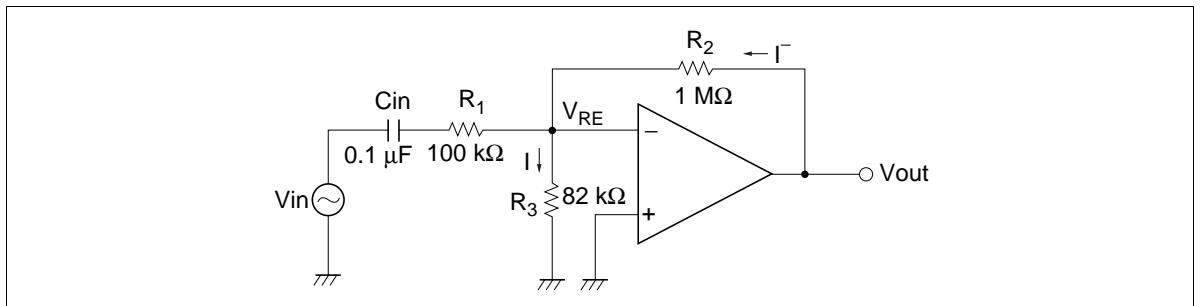
Figure 2 shows a common AC amplifier that is biased by the same power supply as the supply that operates the amplifier.



**Figure 2 Single Power Supply Bias Technique**

$$\frac{V_{out}}{V_{in}} = -\frac{R_2}{R_1} \quad (1)$$

### 2. $NV_{BE}$ Bias Technique



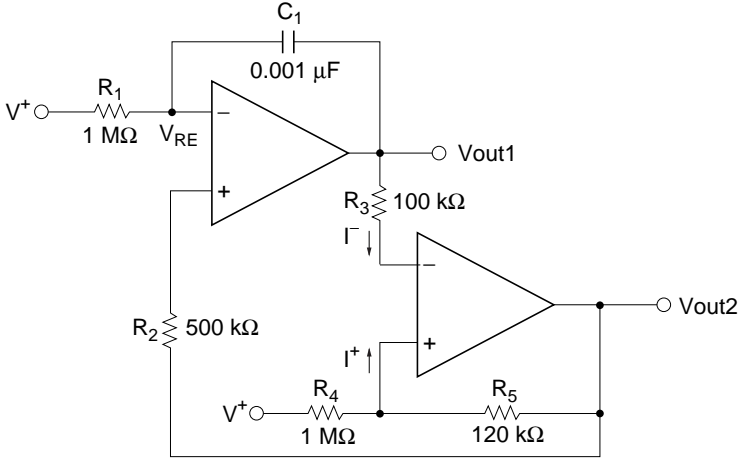
**Figure 3  $NV_{BE}$  Bias Technique**

This is the most useful application of an inverting AC amplifier. In this circuit, the input bias voltage  $V_{BE}$  for the inverting input is determined by the current that flows to ground through the resistor  $R_3$ .

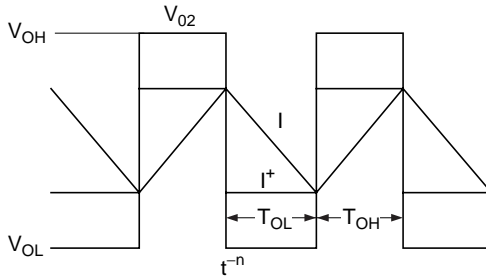
$$\frac{V_{out}}{V_{in}} = -\frac{R_2}{R_1} \quad (2)$$

**Triangular Wave oscillator**

Triangular waveforms are usually acquired by integrating an alternating positive and negative DC voltage. Figure 4 shows the relation between the input and output in this circuit.



**Figure 4 Triangular Wave Oscillator**



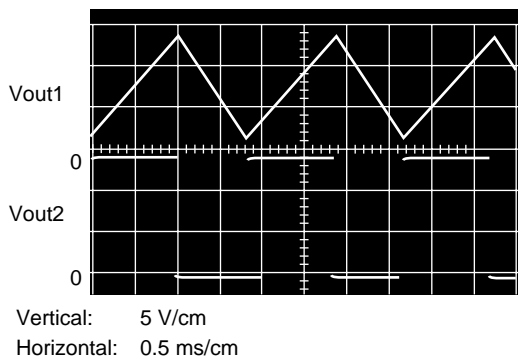
**Figure 5 Triangular Wave Generator Operation**

$$T_{OL} = \frac{C_1 R_1 R_3 V_{OH}}{R_5 (V^+ - V_{BE})} \quad (3)$$

$$T_{OH} = \frac{C_1 R_3 V^+}{R_5 \left( \frac{V_{OH}}{R_2} - \frac{V^+ - V_{BE}}{R_1} \right)} \quad (4)$$

Here, if  $R_1 = 2 \cdot R_2$ ,  $V_{OH} = V^+$ , and  $V^+ > V_{BE}$ , then:

$$T_{OH} + T_{OL} = \frac{2C_1 R_1 R_3}{R_5} \quad (5)$$



**Figure 6 Triangular Wave Generator Operating Waveform**

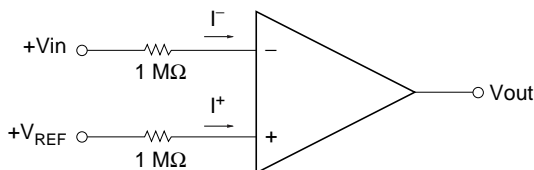
**Table 1**

| Test Item                 |          | Tested Value | Calculated Value | Unit | Test Condition   |
|---------------------------|----------|--------------|------------------|------|--|
| Triangular wave generator | $T_{OH}$ | 1.06         | 0.83             | ms   | $V_{CC} = 15\text{ V}$ , $V^+ = 15\text{ V}$ , $C_1 = 0.001\text{ }\mu\text{F}$ ,    |
|                           | $T_{OL}$ | 0.82         | 0.83             | ms   | $R_1 = 1\text{ M}\Omega$ , $R_2 = 500\text{ k}\Omega$ , $R_3 = 100\text{ k}\Omega$ , |
|                           | $V_{OH}$ | 13.5         | 14               | V    | $R_4 = 1\text{ M}\Omega$ , $R_5 = 120\text{ k}\Omega$                                |
|                           | $V_{OL}$ | 1.5          | 1.5              | V    | Figure 4   |

### Comparators

This section describes three comparator circuits implemented using the HA17301P, a positive input voltage comparator, a negative input voltage comparator, and a power voltage comparator.

#### 1. Positive Input Voltage Comparator



**Figure 7 Positive Input Voltage Comparator**

$V_{out}$  in the circuit shown in figure 7 will be  $V_{OH}$  when  $I^- < I^+$  and  $V_{OL}$  when  $I^- > I^+$ . To assure that this circuit operates correctly, the reference voltage must be greater than  $V_{BE}$ .

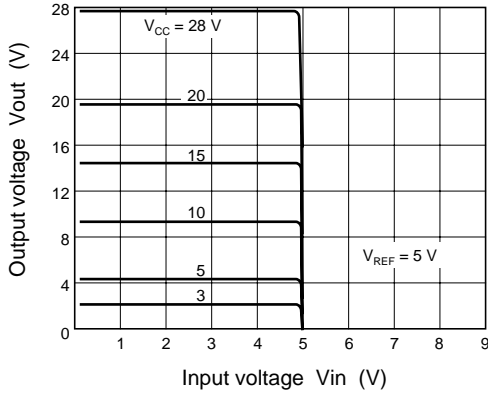


Figure 8 Positive Input Voltage Comparator Operating Characteristics (1)

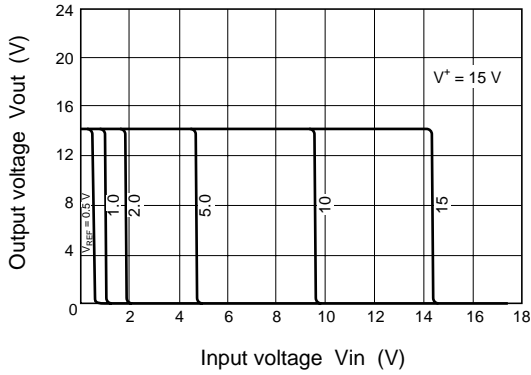


Figure 9 Positive Input Voltage Comparator Operating Characteristics (2)

2. Negative Input Voltage Comparator

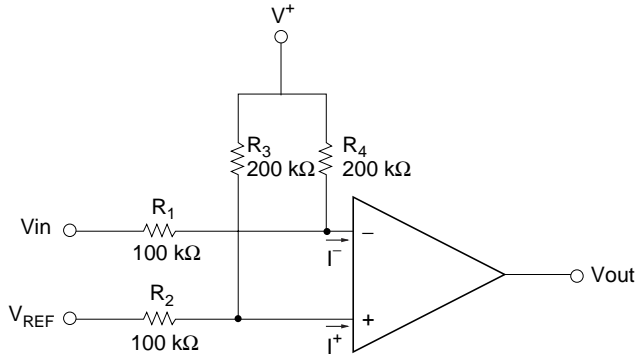


Figure 10 Negative Input Voltage Comparator



$$V_{IN} > R_1 \left\{ V_{BE} \left( \frac{1}{R_1} + \frac{1}{R_4} \right) - \frac{V^+}{R_4} \right\} \quad (6)$$

If resistor  $R_4$  is chosen so that formula 6 holds, and

$$V_{REF} > R_2 \left\{ V_{BE} \left( \frac{1}{R_2} + \frac{1}{R_3} \right) - \frac{V^+}{R_3} \right\} \quad (7)$$

if resistor  $R_4$  is chosen so that formula 7 holds, then even if  $V_{IN}$  and  $V_{REF}$  are negative,  $V_{out}$  will be  $V_{OH}$  when  $\Gamma < \Gamma^+$  and  $V_{OL}$  when  $\Gamma > \Gamma^+$ , as was the case for the positive input voltage comparator.

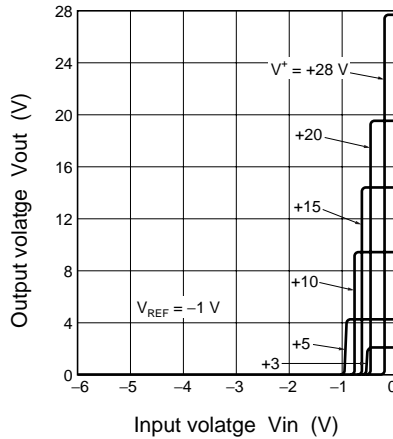


Figure 11 Negative Input Voltage Comparator Operating Characteristics (1)

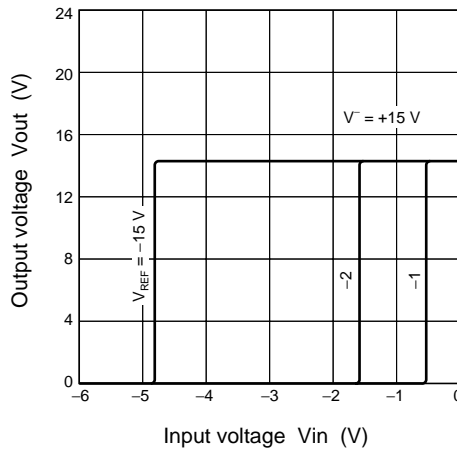
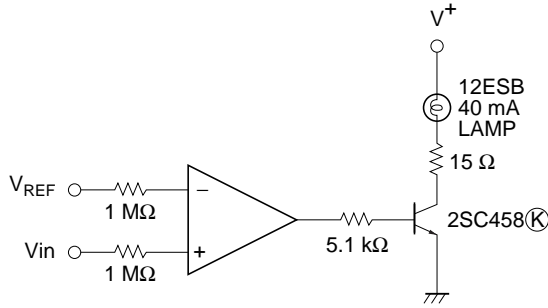


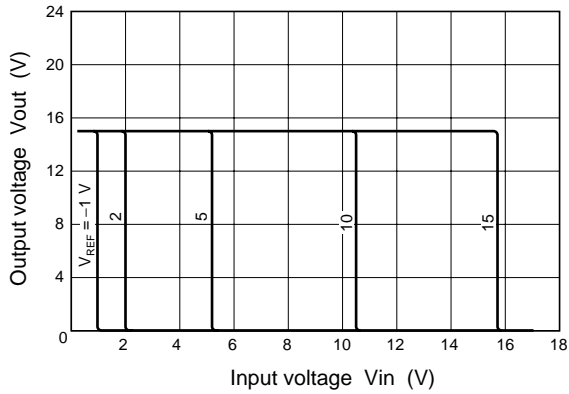
Figure 12 Negative Input Voltage Comparator Operating Characteristics (2)

## 3. Power Comparator

As shown in figure 13, adding an external transistor allows the circuit to drive loads that require a larger current than the output current that the HA17301P can supply.



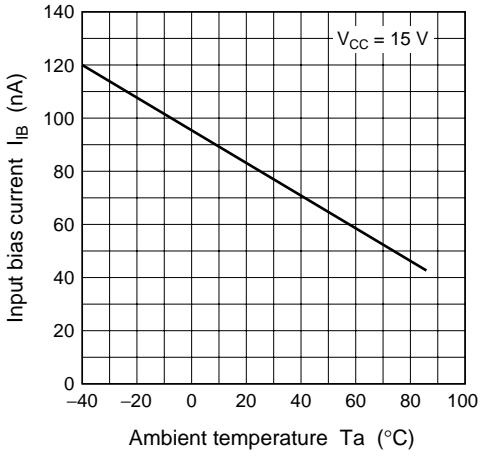
**Figure 13 Power Comparator**



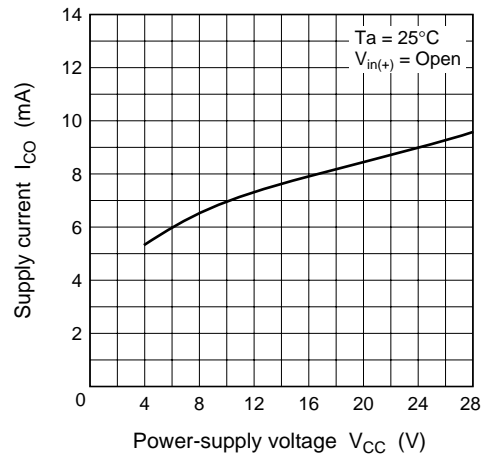
**Figure 14 Power Comparator Operating Characteristics**

Characteristic Curves

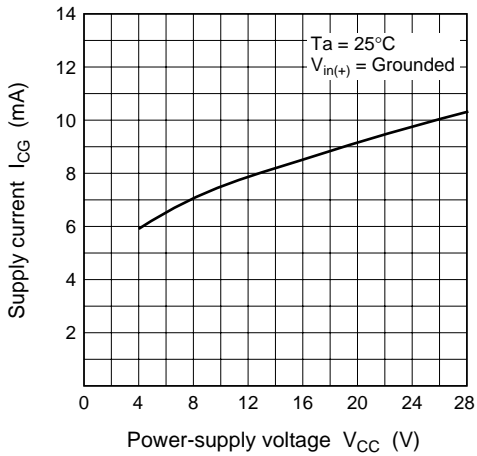
**Input Bias Current vs. Ambient Temperature**



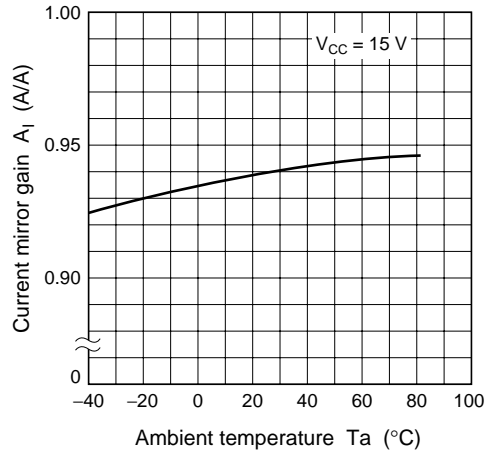
**Supply current vs. Power-Supply Voltage (1)**



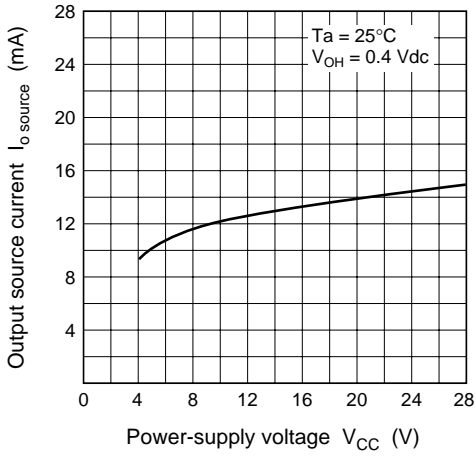
**Supply current vs. Power-Supply Voltage (2)**



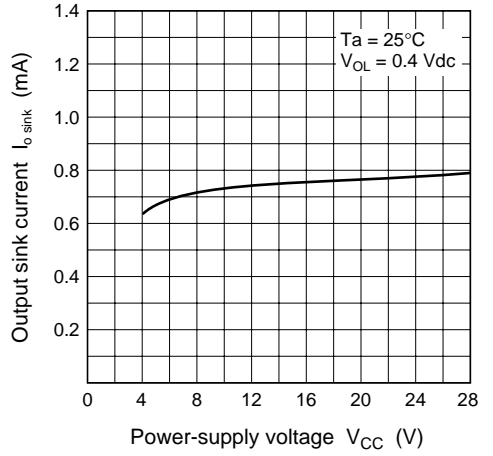
**Current Mirror Gain vs. Ambient Temperature**



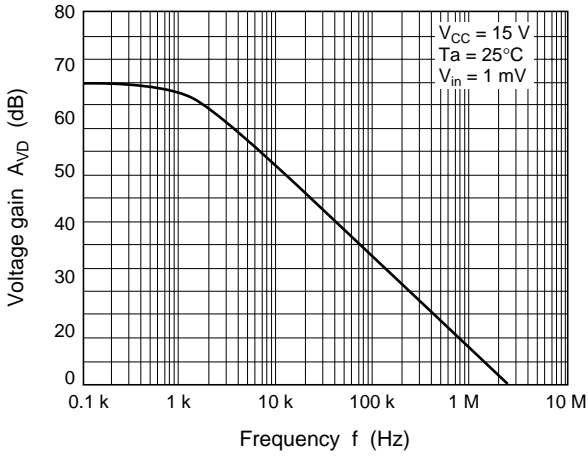
Output Source Current vs. Power-Supply Voltage



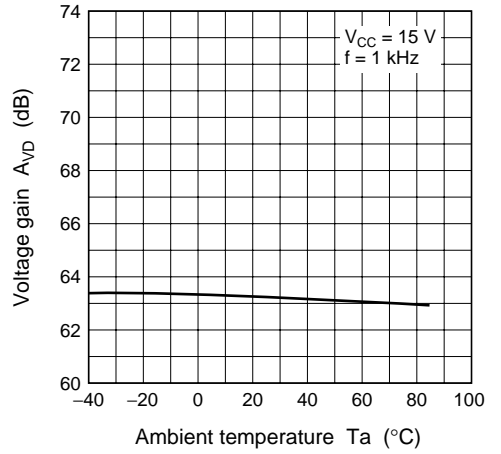
Output Sink Current vs. Power-Supply Voltage



Voltage Gain vs. Frequency

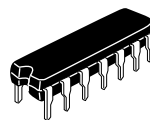
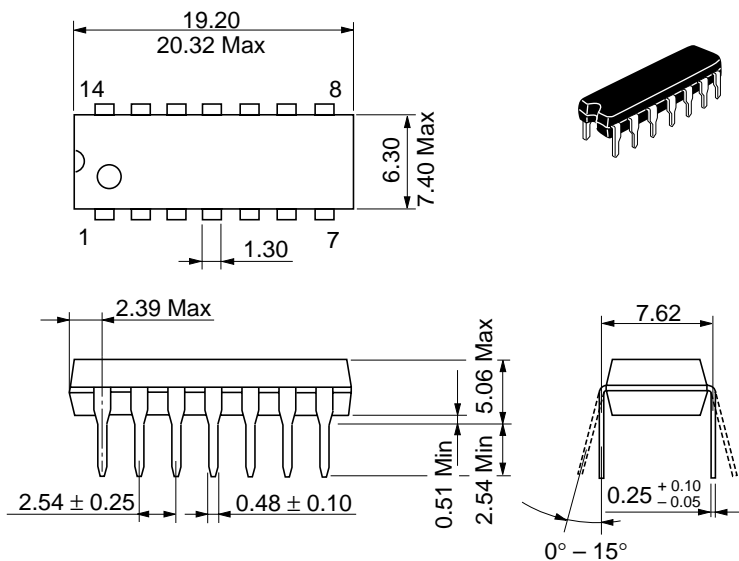


Voltage Gain vs. Ambient Temperature



Package Dimensions

Unit: mm



|                        |          |
|------------------------|----------|
| Hitachi Code           | DP-14    |
| JEDEC                  | Conforms |
| EIAJ                   | Conforms |
| Mass (reference value) | 0.97 g   |

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