## FEATURES

## Low offset voltage: $\mathbf{2 0 0} \mu \mathrm{V}$ maximum

Offset drift: $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ typical
Very low input bias current: 5 pA maximum
Extended temperature range: $-\mathbf{4 0 ^ { \circ }} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
$\pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ dual-supply
Guaranteed GBW: 16 MHz
Voltage noise: 6.1 nV/ل Hz at $1 \mathbf{k H z}$
High slew rate: $60 \mathrm{~V} / \mu \mathrm{s}$
High gain: 120 dB typical
High CMRR: 116 dB typical
High PSRR: 112 dB typical
Low supply current: 7.5 mA maximum

## APPLICATIONS

High impedance sensors
Photo diode amplifier
Precision instrumentation
Phase-locked loop filters
High end, professional audio
DAC output amplifier

## ATE

## Medical

## GENERAL DESCRIPTION

The ADA4627-1 is a wide bandwidth precision amplifier featuring low noise, very low offset, drift, and bias current. Operation is specified from $\pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ dual supply.

The ADA4627-1 provides benefits previously found in few amplifiers. This amplifier combines the best specifications of precision dc and high speed ac op amps.
With a typical offset voltage of only $70 \mu \mathrm{~V}$, drift of less than $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, and noise of only $0.86 \mu \mathrm{~V}$ p-p $(0.1 \mathrm{~Hz}$ to 10 Hz ), the ADA4627-1 is suited for applications in which error sources cannot be tolerated.

The ADA4627-1 is specified for both the industrial temperature range of $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and the extended industrial temper-

## PIN CONFIGURATIONS



Figure 1. 8-Lead SOIC_N (R-8)


NOTES

1. NC = NO CONNECT.
2. CONNECT EXPOSED PAD TO GROUND.

Figure 2. 8-Lead LFCSP_VD (CP-8-2)
ature range of $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. It is available in tiny 8 -lead LFCSP and 8-lead SOIC packages.

The ADA4627-1 is a member of a growing series of high speed, precision op amps offered by Analog Devices, Inc (see Table 1).

Table 1. High Speed Precision Op Amps

| Supply | $\mathbf{5}$ V Low <br> Cost | $\mathbf{5}$ V | $\mathbf{2 6}$ V Low <br> Power | $\mathbf{3 0}$ V Low <br> Cost | 30 V |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Single | AD8615 | AD8651 | AD8610 | AD8510 | ADA4627-1 |
| Dual | AD8616 | AD8652 | AD8620 | AD8512 |  |
| Quad | AD8618 |  |  | AD8513 |  |

Rev. A
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## ADA4627-1

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS—30 V OPERATION

$\mathrm{V}_{\mathrm{SY}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 2.


## ADA4627-1

| Parameter | Symbol | Conditions | B Grade |  |  | A Grade |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max | Min | Typ | Max |  |
| POWER SUPPLY <br> Supply Current per Amplifier | Isy | $\begin{aligned} & \mathrm{lo}=0 \mathrm{~mA} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ |  | $\pm 7.0$ | $\begin{aligned} & \pm 7.5 \\ & \pm 7.8 \end{aligned}$ |  | $\pm 7.0$ | $\begin{aligned} & \pm 7.5 \\ & \pm 7.8 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| OUTPUT CHARACTERISTICS <br> Output Voltage High <br> Output Voltage Low <br> Output Current <br> Short-Circuit Current <br> Closed-Loop Output Impedance | Voн <br> Vo <br> lout <br> Isc <br> Zout | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega \text { to } \mathrm{V}_{\mathrm{CM}} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=1 \mathrm{k} \Omega \text { to } \mathrm{V}_{\mathrm{CM}} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \mathrm{~V}_{\mathrm{O}}= \pm 10 \mathrm{~V} \\ & \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \\ & \mathrm{f}=1 \mathrm{MHz}, A_{V}=-100 \end{aligned}$ | $\begin{aligned} & 12.0 \\ & 11.8 \\ & 11.7 \end{aligned}$ | $\begin{aligned} & 12.3 \\ & -12.7 \\ & \\ & \pm 45 \\ & +70 /-55 \\ & 41 \end{aligned}$ | $\begin{aligned} & -12.3 \\ & -12.1 \\ & -12.0 \end{aligned}$ | $\begin{aligned} & 12.0 \\ & 11.8 \\ & 11.7 \\ & -12.7 \end{aligned}$ | 12.3 $\begin{aligned} & -12.3 \\ & -12.1 \\ & -12.0 \\ & \pm 45 \\ & +70 /-55 \\ & 41 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \Omega \end{aligned}$ |

${ }^{1} V_{\text {os }}$ is measured fully warmed-up.
${ }^{2}$ Tested/extrapolated from $125^{\circ} \mathrm{C}$
${ }^{3}$ Rising/falling.
${ }^{4}$ Not tested. Guaranteed by simulation and characterization.

## ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | 36 V |
| Input Voltage Range $^{1}$ | $(\mathrm{~V}-)-0.3 \mathrm{~V}$ to $(\mathrm{V}+)+0.3 \mathrm{~V}$ |
| Input Current $^{1}$ | $\pm 10 \mathrm{~mA}$ |
| Differential Input Voltage $^{2}$ | $\pm \mathrm{V}_{\text {SY }}$ |
| Output Short-Circuit Duration to GND | Indefinite |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60 sec$)$ | $300^{\circ} \mathrm{C}$ |
| ESD Human Body Model | 2.5 kV |

${ }^{1}$ Input pin has clamp diodes to the power supply pins. Input current should be limited to 10 mA or less whenever input signals exceed the power supply rail by 0.3 V .
${ }^{2}$ Differential input voltage is limited to $\pm 30 \mathrm{~V}$ or the supply voltage, whichever is less.
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

$\theta_{\mathrm{JA}}$ is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages. This was measured using a standard two-layer board. For the LFCSP package, the exposed pad should be soldered to a copper plane.

Table 4. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathbf{J A}}$ | $\boldsymbol{\theta}_{\boldsymbol{\prime} \mathbf{c}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 8-Lead SOIC_N (R-8) | 155 | 45 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead LFCSP (CP-8-2) | 77 | 14 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## ADA4627-1

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 3. Voltage Noise Density


Figure 4. Open-Loop Gain vs. Temperature


Figure 5. CMRR vs. Frequency


Figure 6. Open-Loop Gain and Phase vs. Frequency


Figure 7. Closed-Loop Zout Vs. Frequency


Figure 8. Vos vs. Common-Mode Voltage
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 9. PSRR vs. Frequency


Figure 10. Supply Current vs. Supply Voltage and Temperature


Figure 11. PSRR vs. Temperature


Figure 12. CMRR vs. Temperature


Figure 13. Vout Sinking vs. I LOAD Current


Figure 14. VOUT Sourcing vs. I LOAD Current

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$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 15. Supply Current vs. Supply Voltage


Figure 16. $T H D+N$ vs. $V_{I N}$


Figure 17. Closed-Loop Gain vs. Frequency


Figure 18. $T H D+N$ vs. Frequency


Figure 19. Input Bias Current vs. Temperature


Figure 20. Input Bias Current vs. $V_{C M}$ and Temperature
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 21. Input Bias Current vs. V $\subset M$ at $125^{\circ} \mathrm{C}$


Figure 22. Input Offset Voltage vs. Time


Figure 23. Small Signal Overshoot vs. Load Capacitance


Figure 24. Large Signal Transient Response


Figure 25 Large Signal Transient Response


Figure 26. Large Signal Transient Response

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$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 27. Large Signal Transient Response


Figure 28. Large Signal Transient Response


Figure 29. Small Signal Transient Response


Figure 30. Small Signal Transient Response


Figure 31. Small Signal Transient Response


Figure 32. Small Signal Transient Response
$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 33. No Phase Reversal


Figure 34. Negative Settling Time to 0.01\%


Figure 35. Positive Settling Time to 0.01\%


Figure 36. 0.1 Hz to 10 Hz Noise

## THEORY OF OPERATION

The ADA4627-1 is a high speed, unity gain stable amplifier with excellent dc characteristics. The typical offset voltage of $70 \mu \mathrm{~V}$ allows the amplifier to be easily configured for high gains without the risk of excessive output voltage errors. The small temperature drift of $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ ensures a minimum offset voltage error over the entire temperature range of $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$, making the amplifier ideal for a variety of sensitive measurement applications in harsh operating environments.

## INPUT VOLTAGE RANGE

The ADA4627-1 is not a rail-to-rail input amplifier, thus, care is required to ensure that both inputs do not exceed the input voltage range. Under normal negative feedback operating conditions, the amplifier corrects its output to ensure that the two inputs are at the same voltage. However, if either input exceeds the input voltage range, the loop opens and large currents begin to flow through the ESD protection diodes in the amplifier.
These diodes are connected between the inputs and each supply rail to protect the input transistors against an electrostatic discharge event, and they are normally reverse-biased. However, if the input voltage exceeds the supply voltage, these ESD diodes can become forward-biased. Without current limiting, excessive amounts of current may flow through these diodes, causing permanent damage to the device. If inputs are subject to overvoltage, insert appropriate series resistors to limit the diode current to less than 5 mA .

## INPUT OFFSET VOLTAGE ADJUST RANGE

The ADA4627-1 SOIC package has offset adjust pins for compatibility with some existing designs. The recommended offset nulling circuit is shown in Figure 37.


Figure 37. Standard Offset Null Circuit
With a $100 \mathrm{k} \Omega$ potentiometer, the adjustment range is more than $\pm 11 \mathrm{mV}$. However, the Vos temperature drift increases by several $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ for every millivolt of offset adjust. The ADA4627-1 has matching thin film resistors that are laser trimmed at two temperatures to minimize both offset voltage and offset voltage drift. The offset voltage at room temperature is less than 0.5 mV , and the offset voltage drift is only a few $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ or less, therefore, it is not recommended to use the offset adjust pins, especially for offset adjust of a complete signal
chain. Signal chain offset can be addressed with an autozero amplifier used to form a composite amplifier, or if the ADA4627-1 is at an inverting amplifier stage, it can be modified easily to create a summing amplifier where a potentiometer can be added (see Figure 38). The LFCSP package does not have offset adjust pins.


Figure 38. Alternate Offset Null Circuit for Inverting Stage

## INPUT BIAS CURRENT

Because the ADA4627-1 has a JFET input stage, the input bias current, due to the reverse-biased junction, has a leakage current that approximately doubles every $10^{\circ} \mathrm{C}$. The power dissipation of the part, combined with the thermal resistance of the package, results in the junction temperature increasing 20 to 30 degrees Centigrade above ambient. This parameter is tested with high speed ATE equipment, which does not result in the die temperature reaching equilibrium. This is correlated with bench measurements to match the guaranteed maximum at room temperature in Table 2.
The input current can be reduced by keeping the temperature as low as possible and using a light load on the output.

## NOISE CONSIDERATIONS

The JFET input stage offers very low input voltage noise and input current noise. The thermal noise of a $1 \mathrm{k} \Omega$ resistor at room temperature is $4 \mathrm{nV} / \sqrt{\mathrm{Hz}}$, thus low values of resistance should be used for dc-coupled inverting and noninverting amplifier configurations. In the case of transimpedance amplifiers (TIAs), current noise is more important.
The ADA4627-1 is an excellent choice for both of these applications. Analog Devices offers a wide variety of low voltage noise and low current noise op amps in a variety of processes optimized for different supply voltage ranges. Refer to Application Note AN-940 for a complete discussion of noise, calculations, and selection tables for more than three dozen low noise, op amp families.

## THD + N MEASUREMENTS

Total harmonic distortion plus noise (THD + N) is usually measured with an audio analyzer from Audio Precision, Inc. The analyzer consists of a low distortion oscillator that is swept from the starting frequency to the ending frequency. The
oscillator is connected to the circuit under test, and the output of the circuit goes back to the analyzer.
The analyzer has a tunable notch filter in lock step with the swept oscillator. This removes the fundamental frequency, but allows all of the harmonics and wideband noise to be measured with an integrating voltmeter. However, there is a switchable low-pass filter in series with the notch filter. If the sine wave is at 100 Hz , then the tenth harmonic is still at 1 kHz , thus having a low pass at 80 kHz is not a problem. When the oscillator reaches 20 kHz , the fourth harmonic ( 80 kHz ) is partially attenuated, resulting in a lower reading from the voltmeter. When evaluating THD + N curves from any manufacturer, careful attention should be paid to the test conditions. The difference between an 80 kHz low-pass filter and a 500 kHz filter is shown in Figure 39.


Figure 39. THD $+N$ vs. Frequency

## PRINTED CIRCUIT BOARD LAYOUT, BIAS CURRENT, AND BYPASSING

To take advantage of the very low input bias current of the ADA4627-1 at room temperature, leakage paths must be considered. A printed circuit board, with dust and humidity, can have $100 \mathrm{M} \Omega$ of resistance over a few tenths of an inch. A one mV differential between the two points results in 10 pA of leakage current, more than the guaranteed maximum.

The op amp inputs should be guarded by surrounding the nets with a metal trace maintained at the predicted voltage. In the case of an inverting configuration or transimpedance amplifier, (see Figure 40), the inverting and noninverting nodes can be surrounded by traces held at a quiet analog ground.


Figure 40. Inverting Amplifier with Guard

For a noninverting configuration, the trace can be driven from the feedback divider, but the resistors should be chosen to offer a low impedance drive to the trace (see Figure 41).


Figure 41. Noninverting Amplifier with Guard
The board layout should be compact with traces as short as possible. For second-order board considerations, such as triboelectric effects and piezoelectric effects, as well as a table of insulating material properties, see the AD549 data sheet.
In some cases, shielding from air currents, may be helpful. A general rule of thumb, for op amps with gain bandwidth products higher than 1 MHz , bypass capacitors should be very close to the part, within 3 millimeters. Each supply should be bypassed with a $0.01 \mu \mathrm{~F}$ ceramic capacitor in parallel with a $1 \mu \mathrm{~F}$ bulk decoupling capacitor. The ceramic capacitors should be closer to the op amp. Sockets, which add inductance and capacitance, should not be used.

## OUTPUT PHASE REVERSAL

Output phase reversal occurs in some amplifiers when the input common-mode voltage range is exceeded. As common-mode voltage is moved outside the common-mode range, the outputs of these amplifiers can suddenly jump in the opposite direction to the supply rail. This is the result of the differential input pair shutting down, causing a radical shifting of internal voltages that results in the erratic output behavior.

The ADA4627-1 amplifier has been carefully designed to prevent any output phase reversal if both inputs are maintained within the specified input voltage range. If one or both inputs exceed the input voltage range but remain within the supply rails, an internal loop opens and the output varies. Therefore, the inputs should always be a minimum of 3 V away from either supply rail.

## DRIVING CAPACITIVE LOADS

Adding capacitance to the output of any op amp results in additional phase shift, which reduces stability and leads to overshoot or oscillation. The ADA4627-1 has a high phase margin and low output impedance, so it can drive reasonable values of capacitance. This is a common situation when an amplifier is used to drive the input of switched capacitor ADCs. For other considerations and various circuit solutions, see the Analog Dialogue article titled Ask the Applications Engineer-25, Op Amps Driving Capacitive Loads, available at www.analog.com.

## ADA4627-1

## OUTLINE DIMENSIONS



ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| ADA4627-1ACPZ-R2 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 Lead LFCSP_VD | CP-8-2 | A29 |
| ADA4627-1ACPZ-RL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 Lead LFCSP_VD | CP-8-2 | A29 |
| ADA4627-1ACPZ-R71 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 Lead LFCSP_VD | CP-8-2 | A29 |
| ADA4627-1ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| ADA4627-1ARZ-RL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| ADA4627-1ARZ-R7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| ADA4627-1BRZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| ADA4627-1BRZ-R7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| ADA4627-1BRZ-RL' ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |

[^0]
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## NOTES


[^0]:    ${ }^{1} Z=$ RoHS Compliant Part.

