

# PBL 3772 Dual Stepper Motor Driver

# **Description**

The PBL 3772 is a switch-mode (chopper), constant-current driver IC with two channels, one for each winding of a two-phase stepper motor. The circuit is similar to Ericsson's PBL 3771, but has been designed to generate a minimum amount of power dissipation and can deliver substantially more current to the stepper motor, up to 1000 mA continuously per channel. At 2 x 750 mA output current, power dissipation is only 1.8 W.

The circuit is designed for microstepping applications in conjunction with the matching dual DAC (Digital-to-Analog Converter) PBM 3960/1. A complete driver system consists of these two ICs, a few passive components and a microprocessor for generation of the proper control and data codes required for microstepping.

The PBL 3772 contains a clock oscillator, which is common for both driver channels, a set of comparators and flip-flops implementing the switching control, and two output H-bridges.

Voltage supply requirements are +5 V for logic and +10 to +45 V for the motor. The close match between the two driver channels guarantees consistent output current ratios and motor positioning accuracy.

### **Key Features**

- Dual chopper driver in a single package.
- · Operation at -40 C
- 1000 mA continuous output current per channel.
- Very low power dissipation, 1.8 W at 2 x 750 mA output current.
- Close matching between channels for high microstepping accuracy.
- Specially matched to the Dual DAC PBM 3960.
- Plastic 22-pin batwing DIP package or 28-pin power PLCC with leadframe for heat-sinking through PC board copper.

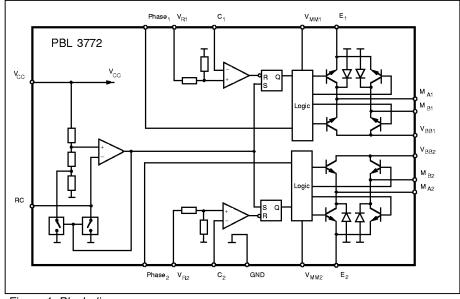
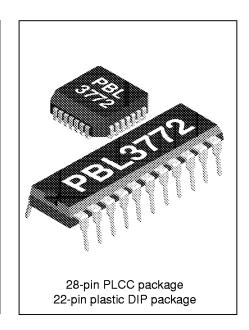


Figure 1. Block diagram.





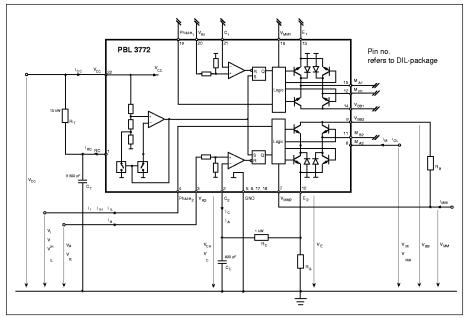
# **Maximum Ratings**

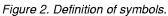
Parameter	Pin no. DIL package	Symbol	Min	Max	Unit
Voltage					
Logic supply	22	V <sub>cc</sub>	0	7	V
Motor supply	7, 16	V <sub>MM</sub>	0	45	V
Output stage supply	9, 14	$V_{\mathtt{BB}}$	0	45	V
Logic inputs	4, 19	$V_{_{\rm I}}$	-0.3	6	V
Comparator inputs	2, 21	V <sub>c</sub>	-0.3	$V_{cc}$	V
Reference inputs	3, 20	V <sub>R</sub>	-0.3	7.5	V
Current					
Motor output current	8, 11, 12, 15	I <sub>M</sub>	-1200	+1200	mA
Logic inputs	4, 19	l <sub>i</sub>	-10		mA
nalog inputs 2, 3, 20, 21		I <sub>A</sub>	-10		mA
Temperature					
Operating junction temperature	T <sub>J</sub>	-40	+150	°C	
Storage temperature		T <sub>s</sub>	-55	+150	°C
Power Dissipation (Package Data	a)				
Power dissipation at $T_{BW} = +25^{\circ}C$ ,	P <sub>D</sub>		5	W	
Power dissipation at T <sub>BW</sub> = +125°C, DIP package		P <sub>D</sub>		2.2	W
Power dissipation at $T_{BW} = +125^{\circ}C$	P <sub>D</sub>		2.6	W	

# **Recommended Operating Conditions**

Parameter	Symbol	Min	Тур	Max	Unit
Logic supply voltage	V <sub>cc</sub>	4.75	5	5.25	V
Motor supply voltage	V <sub>MM</sub>	10		40	٧
Output stage supply voltage	V <sub>BB</sub>	V <sub>MM</sub> - 0.5	5	V <sub>MM</sub>	V
Motor output current	I <sub>M</sub>	-1000		+1000	mA
Junction temperature **	T	-20		+125	°C
Rise and fall time, logic inputs	t <sub>r</sub> , t <sub>r</sub>			2	μs
Oscillator timing resistor	$R_{\tau}$	2	15	20	kΩ

<sup>\*\*</sup> See operating temperature chapter





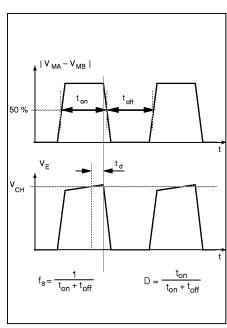


Figure 3. Definition of terms.



### **Electrical Characteristics**

Electrical characteristics over recommended operating conditions, unless otherwise noted. -20°C $\leq$  T<sub>J</sub>  $\leq$  125°C.

Parameter	Symbol	Ref. fig.	Conditions	Min	Тур	Max	Unit
General							
Supply current	I <sub>cc</sub>	2	Note 4.		60	75	mA
Total power dissipation	$P_{D}$	8	$V_{MM} = 12 \text{ V}, I_{M1} = I_{M2} = 750 \text{ mA}.$		1.8	2.1	W
T-t-1		_	R <sub>B</sub> = 0.68 ohm. Notes 2, 3, 4, 5.				14/
Total power dissipation	$P_{D}$	8	$V_{MM} = 12 \text{ V}, I_{M1} = 1000 \text{ mA}, I_{M2} = 0 \text{ mA}.$ $R_{R} = 0.47 \text{ ohm. Notes } 2, 3, 4, 5.$		1.8	2.2	W
Thermal shutdown junction terr	perature	)	В		160		°C
Turn-off delay	t <sub>d</sub>	3	$T_A = +25$ °C, $dV_C/dt \ge 50$ mV/ $\mu$ s, $I_M = 100$ mA. Note 3.		1.4	2.0	μs
Logic Inputs							
Logic HIGH input voltage	V <sub>IH</sub>	2		2.0			V
Logic LOW input voltage	V <sub>IL</sub>	2				0.8	V
Logic HIGH input current	I <sub>IH</sub>	2	V <sub>1</sub> = 2.4 V			20	μΑ
Logic LOW input current	I <sub>IL</sub>	2	V <sub>i</sub> = 0.4 V	-0.4			mA
Comparator Inputs							
Threshold voltage	V <sub>CH</sub>	2	$R_c = 1 \text{ kohm}, V_R = 2.50 \text{ V}$	430	450	470	mV
V <sub>CH1</sub> - V <sub>CH2</sub>   mismatch	V <sub>CH,diff</sub>	2	$R_c = 1 \text{ kohm}$		1		mV
Input current	l <sub>c</sub>	2		-10		1	μΑ
Reference Inputs							
Input resistance	$R_{_{\mathrm{R}}}$		$T_A = +25^{\circ}C$ $V_B = 2.50 \text{ V}$		5		kohm
Input current	I <sub>R</sub>	2	V <sub>R</sub> = 2.50 V		0.5	1.0	mA
Motor Outputs							
Lower transistor saturation volt	age	11	$I_{\rm M} = 750 \text{ mA}$		0.6	0.9	V
Lower transistor leakage current 2		2	$V_{MM} = 41 \text{ V}, V_{E} = V_{R} = 0 \text{ V}, V_{C} = V_{CC}$			700	μΑ
Lower diode forward voltage drop 12		12	$I_{M} = 750 \text{ mA}$		1.2	1.5	V
Upper transistor saturation voltage 13		$I_{\rm M} = 750$ mA. $R_{\rm B} = 0.68$ ohm. Note 5		0.6	0.9	V	
Upper transistor saturation voltage 13		$I_{\rm M} = 750$ mA. $R_{\rm B} = 0.47$ ohm. Note 3, 5		8.0	1.1	V	
Upper transistor leakage current 2			$V_{MM} V_{BB} = 41 V, V_{E} = V_{R} = 0 V, V_{C} = V_{C}$	С		700	μΑ
Chopper Oscillator							
Chopping frequency	f <sub>s</sub>	3	$C_{T} = 3300 \text{ pF}, R_{T} = 15 \text{ kohm}$	25.0	26.5	28.0	kHz

### **Thermal Characteristics**

Parameter	Ref. Symbol fig.	Conditions	Min	Тур	Max	Unit
Thermal resistance	Rth <sub>J-BW</sub>	DIP package		11		°C/W
	Rth <sub>J-A</sub> 14	DIP package. Note 2		40		°C/W
	Rth <sub>J-BW</sub>	PLCC package		9		°C/W
	Rth <sub>J-A</sub> 14	PLCC package. Note 2		35		°C/W

### **Notes**

- 1. All voltages are with respect to ground. Currents are positive into, negative out of specified terminal.
- 2. All ground pins soldered onto a 20 cm $^2$  PCB copper area with free air convection,  $T_A = +25$  $^{\circ}$ C.
- 3. Not covered by final test program.
- 4. Switching duty cycle D = 30%,  $f_s = 26.5 \text{ kHz}$ .
- 5. External resistors  $\boldsymbol{R}_{\mathrm{B}}$  for lowering of saturation voltage.



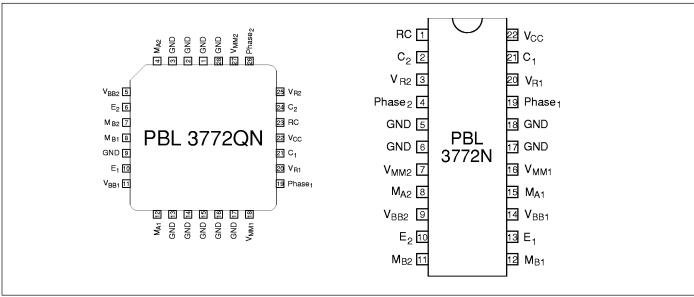


Figure 4. Pin configuration.

# **Pin Description**

PLCC	DIP	Symbol	Description
1-3, 9,	5, 6	GND	Ground and negative supply. Note: these pins are used thermally for heat-sinking.
13-17	17, 18		Make sure that all ground pins are soldered onto a suitably large copper ground
28			plane for efficient heat sinking.
4	8	$M_{A2}$	Motor output A, channel 2. Motor current flows from M <sub>A2</sub> to M <sub>B2</sub> when Phase <sub>2</sub> is HIGH.
5	9	V <sub>BB2</sub>	Collector of upper output transistor, channel 2. For lowest possible power dissipation, connect a series
			resistor R <sub>B2</sub> to V <sub>MM2</sub> . See Applications information, External components.
6	10	E <sub>2</sub>	Common emitter, channel 2. This pin connects to a sensing resistor R <sub>s</sub> to ground.
7	11	$M_{B2}$	Motor output B, channel 2. Motor current flows from M <sub>A2</sub> to M <sub>B2</sub> when Phase <sub>2</sub> is HIGH.
8	12	$M_{B1}$	Motor output B, channel 1. Motor current flows from M <sub>A1</sub> to M <sub>B1</sub> when Phase, is HIGH.
10	13	E,	Common emitter, channel 1. This pin connects to a sensing resistor R <sub>s</sub> to ground.
11	14	$V_{_{\mathrm{BB1}}}$	Collector of upper output transistor, channel 1. For lowest possible power dissipation, connect a series
			resistor R <sub>B1</sub> to V <sub>MM1</sub> . See Applications information, External components.
12	15	$M_{A1}$	Motor output A, channel 1. Motor current flows from M <sub>A1</sub> to M <sub>B1</sub> when Phase <sub>1</sub> is HIGH.
18	16	$V_{MM1}$	Motor supply voltage, channel 1, +10 to +40 V. $V_{\rm MM1}$ and $V_{\rm MM2}$ should be connected together.
19	19	Phase₁	Controls the direction of motor current at outputs $M_{A1}$ and $M_{B1}$ . Motor current flows from $M_{A1}$ to $M_{B1}$
			when Phase₁ is HIGH.
20	20	$V_{_{\mathrm{R1}}}$	Reference voltage, channel 1. Controls the threshold voltage for the comparator and hence the output
			current.
21	21	C <sub>1</sub>	Comparator input channel 1. This input senses the instantaneous voltage across the sensing resistor,
			filtered by an RC network. The threshold voltage for the comparator is $V_{CH1} = 0.18 \cdot V_{R1}$ [V], i.e. 450
			mV at $V_{R1} = 2.5 \text{ V}$ .
22	22	$V_{cc}$	Logic voltage supply, nominally +5 V.
23	1	RC	Clock oscillator RC pin. Connect a 15 kohm resistor to $V_{cc}$ and a 3300 pF capacitor to ground to
			obtain the nominal switching frequency of 26.5 kHz.
24	2	$C_2$	Comparator input channel 2. This input senses the instantaneous voltage across the sensing resistor,
			filtered by an RC network. The threshold voltage for the comparator is $V_{CH2} = 0.18 \cdot V_{R2}$ [V], i.e. 450 mV
			at $V_{R2} = 2.5 \text{ V}$ .
25	3	$V_{_{\mathrm{R2}}}$	Reference voltage, channel 2. Controls the threshold voltage for the comparator and hence the output
			current.
26	4	Phase <sub>2</sub>	Controls the direction of motor current at outputs $M_{A2}$ and $M_{B2}$ . Motor current flows from $M_{A2}$ to $M_{B2}$
	_		when Phase <sub>2</sub> is HIGH.
27	7	$V_{_{\rm MM2}}$	Motor supply voltage, channel 2, +10 to +40 $V.V_{MM1}$ and $V_{MM2}$ should be connected together.



### **Functional Description**

Each channel of the PBL 3772 consists of the following sections: an output H-bridge with four transistors, capable of driving up to 1000 mA continuous current to the motor winding; a logic section that controls the output transistors; an S-R flip-flop; and a comparator. The clock-oscillator is common to both channels.

Constant current control is achieved by switching the output current to the windings. This is done by sensing the peak current through the winding via a current-sensing resistor R<sub>s</sub>, effectively connected in series with the motor winding during the turn-on period. As the current increases, a voltage develops across the sensing resistor, which is fed back to the comparator. At the predetermined level, defined by the voltage at the reference input V<sub>B</sub>, the comparator resets the flip-flop, which turns off the output transistors. The current decreases until the clock oscillator triggers the flip-flop, which turns on the output transistors again, and the cycle is repeated.

The current paths during turn-on, turn-off and phase shift are shown in figure 5. Note that the upper recirculation diodes are connected to the circuit externally.

## **Applications Information**

#### **Current control**

The output current to the motor winding is determined by the voltage at the reference input and the sensing resistor, R<sub>o</sub>.

Chopping frequency, winding inductance and supply voltage also affect the current, but to much less extent.

The peak current through the sensing resistor (and motor winding) can be expressed as:

$$\begin{split} &I_{\text{M,peak}} = 0.18 \bullet (\text{ V}_{\text{R}} / \text{ R}_{\text{S}}) \quad [\text{A}] \\ &\text{i.e., with a recommended value of} \\ &0.47 \text{ ohm for the sensing resistor R}_{\text{S}}, \text{ a} \\ &2.5 \text{ V reference voltage will produce an} \\ &\text{output current of approximately 960 mA.} \\ &\text{To improve noise immunity on the V}_{\text{R}} \\ &\text{input, the control range may be} \\ &\text{increased to 5 V if R}_{\text{S}} \text{ is correspondingly changed to 1 ohm.} \end{split}$$

#### **External components**

The PBL 3772 exhibits substantially less power dissipation than most other comparable stepper motor driver ICs on the market. This has been achieved by creating an external voltage drop in series with the upper transistor in the output H-bridge, see figure 5. The voltage drop reduces the collectoremitter saturation voltage of the internal transistor, which can greatly reduce power dissipation of the IC itself. The series resistor, designated  $R_{\rm g}$ , shall be selected for about 0.5 V voltage drop at the maximum output current. In an application with an output current of 1000 mA (peak), a 0.47 ohm. 1/2 W resistor is the best choice.

In low current applications where power dissipation is not a critical factor, the  $\rm R_{\rm B}$  resistor can of course be omitted, and the  $\rm V_{\rm MM}$  and  $\rm V_{\rm BB}$  pins (pins 5, 11, 18, 27) can all be connected directly to the motor supply voltage  $\rm V_{\rm MM}$ .

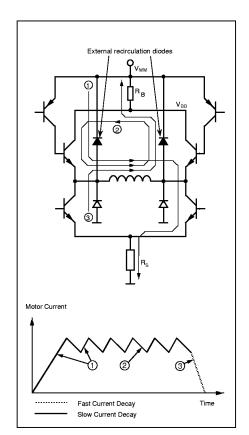


Figure 5. Output stage with current paths during turn-on, turn-off and phase shift.

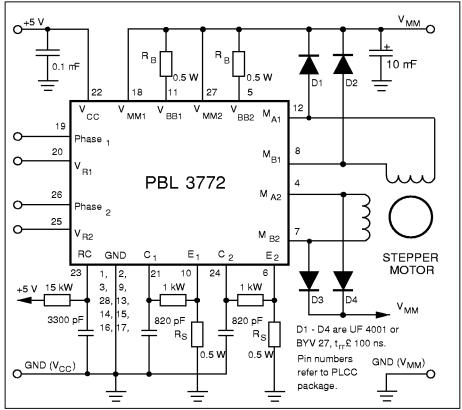


Figure 6. Typical stepper motor driver application with PBL 3772.



Contributing to the low power dissipation is the fact that the upper recirculation diodes in the output H-bridge are connected externally to the circuit. These diodes shall be of fast type, with a t<sub>rr</sub> of less than 100 ns. Common types are UF4001 or BYV27.

A low pass filter in series with the comparator input prevents erroneous switching due to switching transients. The recommended filter component values, 1 kohm and 820 pF, are suitable for a wide range of motors and operational conditions.

Since the low-pass filtering action introduces a small delay of the signal to the comparator, peak voltage across the sensing resistor, and hence the peak motor current, will reach a slightly higher level than than what is defined by the comparator threshold,  $V_{CH}$ , set by the reference input  $V_{R}$  ( $V_{CH}$  = 450 mV at  $V_{R}$  = 2.5 V).

The time constant of the low-pass filter may therefore be reduced to minimize the delay and optimize low-current

perform-ance. Increasing the time constant may result in unstable switching. The time constant should be adjusted by changing the  $C_{\rm c}$  value.

The frequency of the clock oscillator is set by the  $R_{\tau}\text{-}C_{\tau}$  timing components at the RC pin. The recommended values result in a clock frequency (= switching frequency) of 26.5 kHz. A lower frequency will result in higher current ripple, but may improve low-current level linearity. A higher clock frequency reduces current ripple, but increases the switching losses in the IC and possibly the iron losses in the motor. If the clock frequency needs to be changed, the  $C_{\tau}$  capacitor value should be adjusted. The recommended  $R_{\tau}$  resistor value is 15 kohm.

The sensing resistor  $R_{\rm s}$ , should be selected for maximum motor current. The relationship between peak motor current, reference voltage and the value of  $R_{\rm s}$  is described under Current control above. Be sure not to exceed the maximum output current which is

1200 mA peak when only one channel is activated. Or recommended output current, which is 1000 mA peak, when both channels is activated.

#### Motor selection

The PBL 3772 is designed for twophase bipolar stepper motors, i.e., motors that have only one winding per phase.

The chopping principle of the PBL 3772 is based on a constant frequency and a varying duty cycle. This scheme imposes certain restrictions on motor selection. Unstable chopping can occur if the chopping duty cycle exceeds approximately 50%. See figure 3 for definitions. To avoid this, it is necessary to choose a motor with a low winding resistance and inductance, i.e. windings with a few turns.

It is not possible to use a motor that is rated for the same voltage as the actual supply voltage. Only rated current needs to be considered. Typical motors to be used together with the PBL 3772 have a

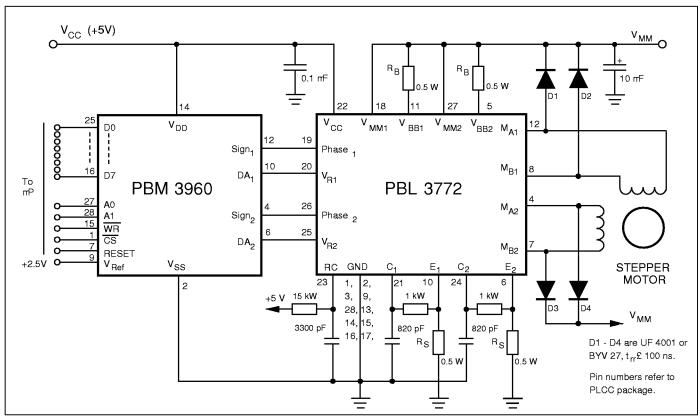


Figure 7. Microstepping system with PBM 3960 and PBL 3772.



voltage rating of 1 to 6 V, while the supply voltage usually ranges from 12 to 40 V.

Low inductance, especially in combination with a high supply voltage, enables high stepping rates. However, to give the same torque capability at low speed, a reduced number of turns in the winding must be compensated by a higher current. A compromise has to be made.

Choose a motor with the lowest possible winding resistance that still gives the required torque, and use as high supply voltage as possible, without exceeding the maximum recommended 40 V. Check that the chopping duty cycle does not exceed 50% at maximum current.

#### General

**Phase inputs.** A logic HIGH on a Phase input gives a current flowing from pin  $M_A$  into pin  $M_B$ . A logic LOW gives a current flow in the opposite direction. A time delay prevents cross conduction in the H-bridge when changing the Phase input.

**Heat sinking.** Soldering the batwing ground leads onto a copper ground plane of 20 cm² (approx. 1.8" x 1.8"), copper foil thickness 35  $\mu$ m, permits the circuit to operate with 750 mA output current, both channels driving, at ambient temperatures up to 70°C. Consult figures 8, 9, 10 and 14 in order to determine the necessary copper ground plane area for heat sinking at higher current levels.

**Thermal shutdown.** The circuit is equipped with a thermal shutdown function that turns the output off at chip temperatures above 160°C. Normal operation is resumed when the temperature has decreased about 20°C.

Operating temperature. The max recommended operating temperature is 125°C. This gives an estimated lifelength of about 5 years at continous drive, A change of  $\pm 10^\circ$  would increase/decrease the lifelength of the circuit about 5 years.

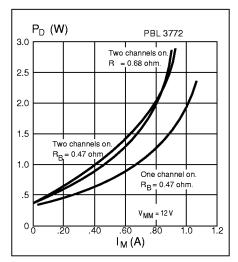


Figure 8. Power dissipation vs. motor current. $T_a = 25$ °C.

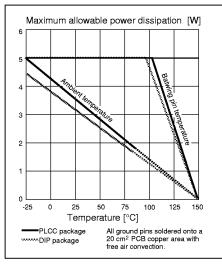


Figure 10. Maximum allowable power dissipation vs. temperature.

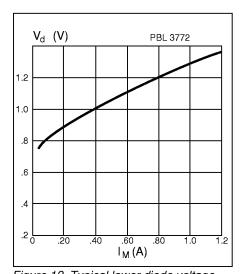


Figure 12. Typical lower diode voltage drop vs. recirculating current.

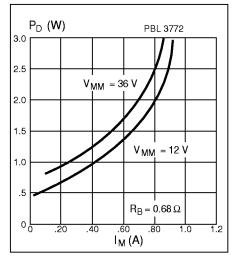


Figure 9. Power dissipation vs. motor current, both channels on  $T_2 = 25$ °C.

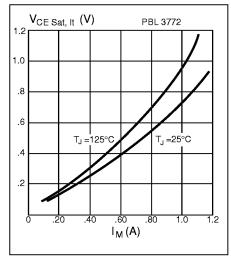


Figure 11. Typical lower transistor saturation voltage vs. output current.

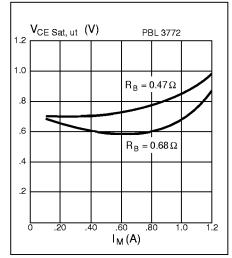


Figure 13. Typical upper transistor saturation voltage vs. output current.



# **Ordering Information**

PackagePart No.DIPPBL3772NPLCCPBL3772QNPLCC Tape & ReelPBL3772QN:T

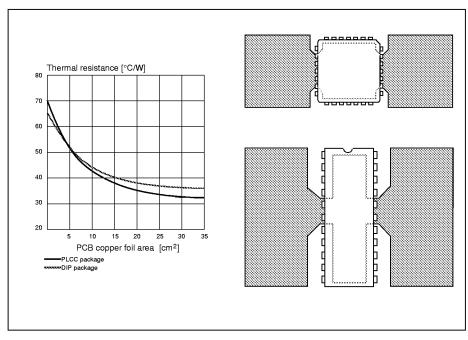


Figure 14. Typical thermal resistance vs. PC Board copper area and suggested layout.

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