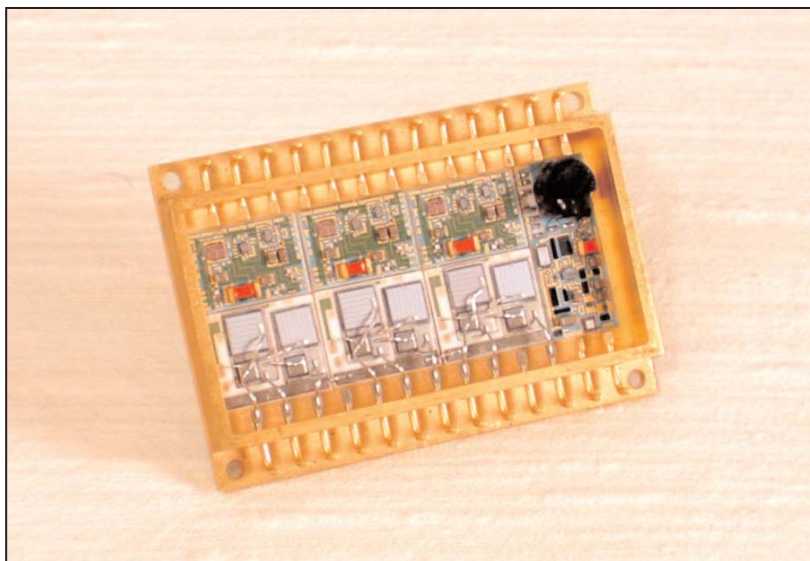


# PWR-82331 AND PWR-82333 SMART POWER 3-PHASE MOTOR DRIVES

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## FEATURES

- Small Size (3.0" x 2.1" x 0.39")
- +200 V and +500 V Capability
- 30 A Current Capability
- High-Efficiency MOSFET or IGBT Drive Stage
- Direct Drive from Commutation Logic
- Six Step Trapezoidal or Sinusoidal Drive
- Four Quadrant Operation
- 0.85° C/W  $\theta_{JC}$  Max
- Military Processing Available

## DESCRIPTION

The PWR-82331 and PWR-82333 are 30 A, 3-phase motor drive hybrids. The PWR-82331 has a +200 V rating and uses MOSFETs in the output stage while the PWR-82333 has a +500 V rating and an IGBT output stage. Both types have individual fast recovery diodes internally connected across the output drive transistors to clamp inductive flyback. These Smart Power Motor Drives have CMOS Schmitt Trigger inputs for high noise immunity. High- and low-side input logic signals are XOR'd in each phase to prevent simultaneous turn-on of in-line transistors, thus eliminating a shoot through condition. The internal logic controls the high- and low-side gate drives for each phase and can operate from +5 to +15 V logic levels. The internal power supply provides a constant voltage source to the floating high-side gate drives, and constant output performance for switching frequencies from dc to 50 kHz.

## APPLICATIONS

These hybrids are an excellent choice for high-performance, high-reliability motor drives for Military and Aerospace servo-amps and speed controls. Among the many applications are robotics; electro-mechanical valve assemblies; actuator systems for flight control surfaces on military and commercial aircraft; antenna and radar positioning; fan and blower motors for environmental conditioning; thrust and vector position control of mini-sub, drones, and RPV's; compressor motors for cryogenic coolers; and high power inverters.

The PWR-82331/82333 hybrids are ideal for harsh military environments where shock, vibration, and temperature extremes are evident, such as missile applications where fin actuator systems control missile direction.

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PWR-82331 PWR-82333

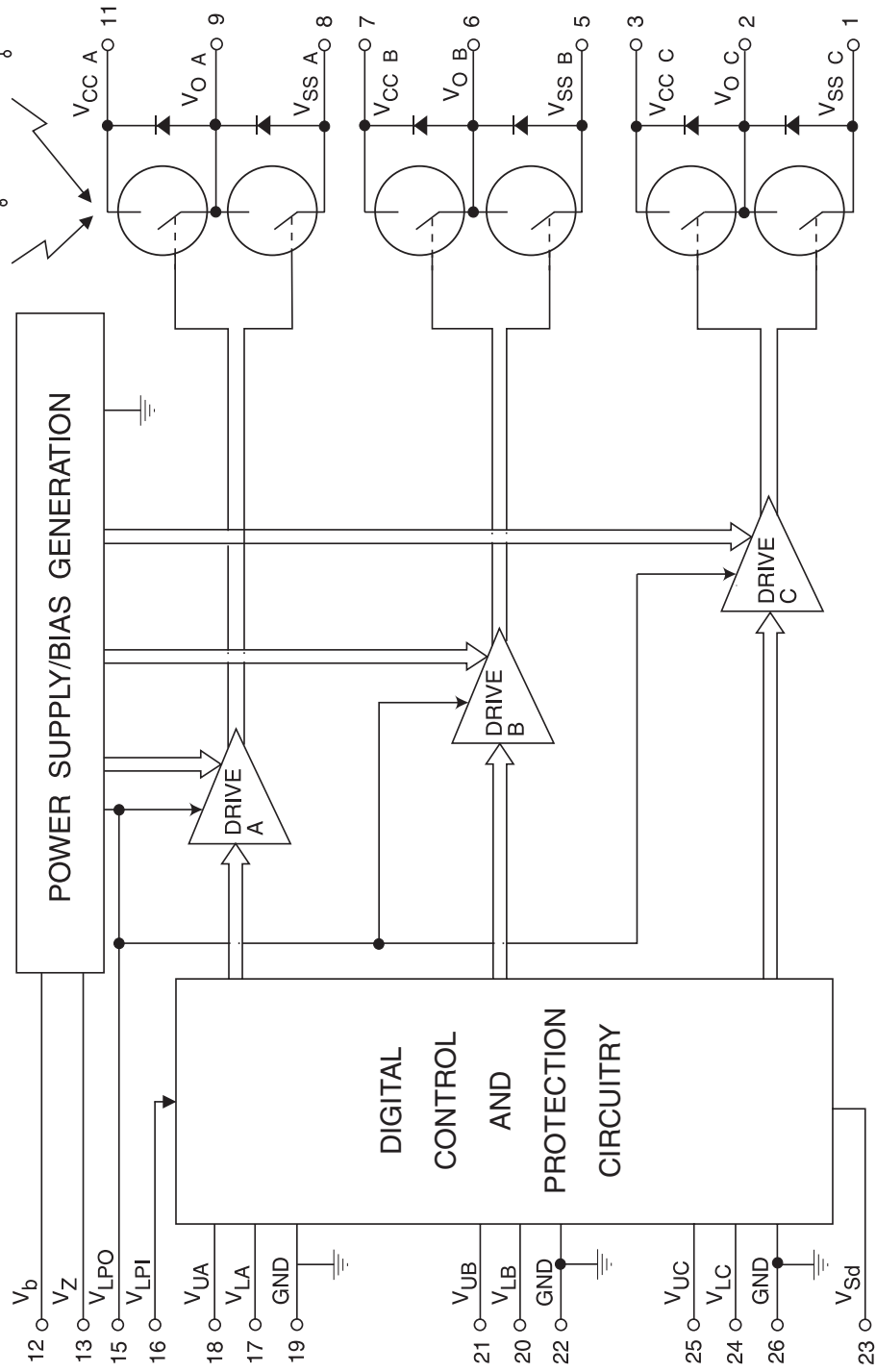


FIGURE 1. PWR-82331/82333 BLOCK DIAGRAM

**TABLE 1. PWR-82331 AND PWR-82333 ABSOLUTE MAXIMUM RATINGS  
(TC = +25°C UNLESS OTHERWISE SPECIFIED)**

PARAMETER	SYMBOL	PWR-82331	PWR-82333	UNITS
SUPPLY VOLTAGE	V <sub>CC</sub>	200	500	V
BIAS VOLTAGE	V <sub>B</sub>	50	50	V
LOGIC POWER-IN VOLTAGE	V <sub>LPI</sub>	18	18	V
INPUT LOGIC VOLTAGE	V <sub>U</sub> , V <sub>L</sub> , V <sub>Sd</sub>	V <sub>LPI</sub> + 0.5	V <sub>LPI</sub> + 0.5	V
OUTPUT CURRENT				
Continuous	I <sub>o</sub>	30	30	A
Pulsed	I <sub>oP</sub>	50	50	A
OPERATING FREQUENCY	f <sub>o</sub>	50	25	kHz
CASE OPERATING TEMPERATURE	T <sub>C</sub>	-55 to +125	-55 to +125	°C
CASE STORAGE TEMPERATURE RANGE	T <sub>CS</sub>	-55 to +150	-55 to +150	°C
GND - VSS DIFFERENTIAL VOLTAGE		± 3	± 3	V <sub>dc-peak</sub>

**TABLE 2. PWR-82331 AND PWR-82333 SPECIFICATIONS  
(TC = +25°C UNLESS OTHERWISE SPECIFIED)**

PARAMETER	SYMBOL	TEST CONDITIONS	PWR-82331			PWR-82333			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
<b>OUTPUT</b>									
Output Current Continuous (see FIG.'s 15 & 19)	I <sub>o</sub>				30			30	A
Supply Voltage	V <sub>CC</sub>	see note 1		28	140		270	350	V
Output On-Resistance (each FET)(see FIG. 14A)	R <sub>ON</sub>	I <sub>o</sub> =30 A			0.1				ohm
Output Voltage drop (each IGBT) (see FIG. 14B)	V <sub>CE(SAT)</sub>	I <sub>o</sub> =30 A						3.8	V
Instant Forward Voltage (flyback diode) (see FIG.'s 13A/B)	V <sub>F</sub>	I <sub>oP</sub> =30 A, see note 2			1.15			1.70	V
Reverse Recovery Time (flyback diode)	t <sub>rr</sub>	I <sub>f</sub> =1 A, I <sub>r</sub> =1 A			50			50	nsec
Reverse Leakage Current at TC = +25°C	I <sub>r</sub>	see note 3			10			10	µA
Reverse Leakage Current at TC = +125°C	I <sub>r</sub>	see note 3			1			1	mA
<b>BIAS SUPPLY</b>									
Input Bias Voltage (T <sub>C</sub> = -55°C to +125°C)	V <sub>b</sub>		14		50	14		50	V
Quiescent Bias Current (see note 4)(see FIG. 16)	I <sub>bq</sub>	V <sub>b</sub> = 28 V		32			32		mA
Bias Current (T <sub>C</sub> = -55°C to +125°C)(see FIG.'s 17 & 18)	I <sub>b</sub>	V <sub>b</sub> =28 V, see note 5	35		65	35		65	mA
In-rush Current (T <sub>C</sub> = -55°C to +125°C)	I <sub>ir</sub>	V <sub>b</sub> = 28 V			1.4			1.4	A
Logic power Input Current	I <sub>LPI</sub>	see note 6			2			2	mA
<b>INPUT SIGNALS (SEE FIG. 7)</b>		<b>Pin Connections</b>							
Positive Trigger Threshold Voltage	V <sub>P</sub>	Pin 15 & 16 connect.			12.9			12.9	V
Negative Trigger Threshold Voltage	V <sub>N</sub>	Pin 15 & 16 connect.	2.1			2.1			V
Hysteresis Voltage	V <sub>H</sub>	Pin 15 & 16 connect	1.6		10.8	1.6		10.8	V
Positive Trigger Threshold Voltage	V <sub>P</sub>	See note 6			4.3			4.3	V
Negative Trigger Threshold Voltage	V <sub>N</sub>	See note 6	0.9			0.9			V
Hysteresis Voltage	V <sub>H</sub>	See note 6	0.3		3.6	0.3		3.6	V
<b>SWITCHING CHARACTERISTICS (SEE FIG. 2)</b>		<b>Test 1 Conditions</b>							
Upper Drive:		Pin 15 & 16 connect.							
Turn-on propagation delay	t <sub>d(on)</sub>	+15 V Logic			840			810	nsec
Turn-off propagation delay	t <sub>d(off)</sub>	I <sub>o</sub> =30 A peak			1020			860	nsec
Shut-down propagation delay	t <sub>Sd</sub>				800			810	nsec
Turn-on Rise Time	t <sub>r</sub>	PWR-82331,			125			100	nsec
Turn-off Fall Time	t <sub>f</sub>	V <sub>CC</sub> = 140 V			125			150	nsec
Lower Drive:		PWR-82333,							
Turn-on propagation delay	t <sub>d(on)</sub>	V <sub>CC</sub> = 270 V			850			800	nsec
Turn-off propagation delay	t <sub>d(off)</sub>				1000			870	nsec
Shut-down propagation delay	t <sub>Sd</sub>				800			770	nsec
Turn-on Rise Time	t <sub>r</sub>				125			100	nsec
Turn-off Fall Time	t <sub>f</sub>				125			150	nsec
<b>SWITCHING CHARACTERISTICS (SEE FIG. 2)</b>		<b>Test 2 Conditions</b>							
Upper Drive:		see note 6							
Turn-on propagation delay	t <sub>d(on)</sub>	+5 V, I <sub>o</sub> =30 A peak			1090			1050	nsec
Turn-off propagation delay	t <sub>d(off)</sub>	PWR-82331,			1315			1150	nsec
Shut-down propagation delay	t <sub>Sd</sub>	V <sub>CC</sub> = 140 V			1100			850	nsec
Turn-on Rise Time	t <sub>r</sub>				125			100	nsec
Turn-off Fall Time	t <sub>f</sub>	PWR-82333,			125			150	nsec
		V <sub>CC</sub> = 270 V							

**TABLE 2. PWR-82331 AND PWR-82333 SPECIFICATIONS (CONT'D)**  
(TC = +25°C UNLESS OTHERWISE SPECIFIED)

PARAMETER	SYMBOL	TEST CONDITIONS	PWR-82331			PWR-82333			UNIT
			MIN	TYP	MAX	MIN	TYP	MAX	
<b>SWITCHING CHARACTERISTICS (CONT'D)</b>									
Lower Drive:		<b>Test 2 Conditions</b> see note 6 +5 V, I <sub>o</sub> =30 A peak			1125			1050	nsec
Turn-on Propagation delay	t <sub>d(on)</sub>	PWR-82331, V <sub>cc</sub> =140 V  PWR-82333, 270 V			1290			1150	nsec
Turn-off Propagation delay	t <sub>d(off)</sub>				1100			850	nsec
Shut-down propagation delay (see FIG. 10)	t <sub>sd</sub>				125			100	nsec
Turn-on Rise Time	t <sub>r</sub>				125			150	nsec
Turn-off Fall Time	t <sub>f</sub>								
<b>DEAD TIME</b>	t <sub>dt</sub>		400			500			nsec
<b>MINIMUM PULSE WIDTH</b>	t <sub>pw</sub>		150			150			nsec
<b>THERMAL</b>									
Maximum Thermal Resistance	θ <sub>jc</sub>	each transistor			0.85			0.85	°C/W
Maximum Lead Soldering Temperature (Note 7)	T <sub>s</sub>				250			250	°C
Junction Temperature Range	T <sub>j</sub>		-55		150	-55		150	°C
Case Operating Temperature	T <sub>co</sub>		-55		125	-55		125	°C
Case Storage Temperature	T <sub>cs</sub>		-55		150	-55		150	°C
<b>WEIGHT</b>									
					4.9 (140)			4.9 (140)	oz (g)

Notes:

1. For Hi-Rel applications, derating per MIL-S-19500 should be observed. (Derate V<sub>cc</sub> to 70%.)
2. Pulse width ≤ 300 ms, duty cycle ≤ 2%.
3. For PWR-82331, V<sub>cc</sub> = 140 V, V<sub>U</sub>, V<sub>L</sub> = Logic '0' and for PWR-82333, V<sub>cc</sub> = 350 V, V<sub>U</sub>, V<sub>L</sub> = Logic '0'.
4. V<sub>U</sub>, V<sub>L</sub> = Logic '0' on pins 17, 18, 20, 21, 24 and 25.
5. For PWR-82331, f<sub>o</sub> = 30 kHz and for PWR-82333, f<sub>o</sub> = 10 kHz.
6. Pin 16 connected to external +5 V supply.
7. Solder 1/8" from case for 5 seconds maximum.

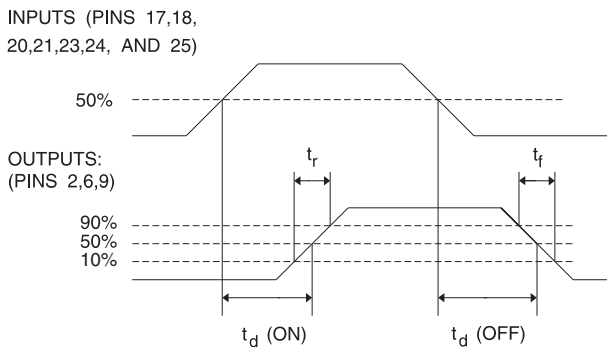
**INTRODUCTION**

The 3-phase PWR-82331 and PWR-82333 are 30 A motor drive hybrids rated at +200 V and +500 V respectively. The PWR-82331 uses a MOSFET output stage and the PWR-82333 has an IGBT output stage for high speed, high current, and high efficiency operation. The PWR-82333 also offers high-voltage performance of an IGBT for use in +270 V systems. These motor drives are ideal for use in high-performance motion control systems, servo amplifiers, and motor speed control designs. Furthermore, multi-axis systems requiring multiple drive stages can benefit from the small size of these power drives.

The PWR-82331/82333 can be driven directly from the commutation logic, DSP, or a custom ASIC that supplies digital signals to control the upper and lower transistors of each phase. These highly integrated drive stages have Schmitt trigger digital inputs

that control the high and low side of each phase. Digital protection of each phase eliminates an in-line firing condition by preventing simultaneous turn-on of both the upper and lower transistors. The logic controls the high- and low-side gate drivers. Operation from +5 to +15 V logic levels can be programmed by applying the appropriate voltage to pin 16 (VLPI). The PWR-82331/82333 has a ground referenced low-side gate drive. An internal dc-dc converter supplies a floating output to each side of the three high-side drives. This provides a continuous high-side gate drive even during the motor stall. Pin 15 (VLPO) supplies a +15 V output, which can be used to power the internal logic when system usage requires +15 V logic. The high- and low-side gate drivers control the N-channel MOSFET or IGBT output stage.

The MOSFETs used in the PWR-82331 allow output switching up to 50 kHz, while the high-speed IGBTs in the PWR-82333 can switch at 25 kHz. A flyback diode parallels each output transistor and controls the regenerative energy produced by the motor. These fast recovery diodes have faster reverse switching times than the intrinsic body diode of the MOSFETs used in the PWR-82331. They also protect the IGBTs used in the PWR-82333 from exceeding their emitter-to-collector breakdown voltage. Use of a copper case and solder attachment of the output transistors achieves a low thermal resistance of 0.85° C/W maximum. Care should be taken to adequately heatsink these motor drives to maintain a case temperature of 125°C. Junction temperatures should not exceed 150°C. The PWR-82331/82333 do not have internal short-circuit or overcurrent protection. For protection of the output transistors, these features must be added externally to the hybrid.



(REFERENCE TABLE 2. ALSO.)

**FIGURE 2. INPUT/OUTPUT TIMING RELATIONSHIPS**

## BIAS VOLTAGES

The PWR-82331/82333 motor drive hybrids require only a single power supply for operation. The hybrid generates three independent floating supplies, eliminating the need for external bias voltages for each phase.

In order for the internal power supply to generate these voltages, the input bias voltage ( $V_b$ ) must be from +15 to +50 Vdc. In most avionic systems this can be accomplished by connecting the  $V_b$  pin to the MIL-STD-704D, +28 Volt bus. See FIGURE 3A.

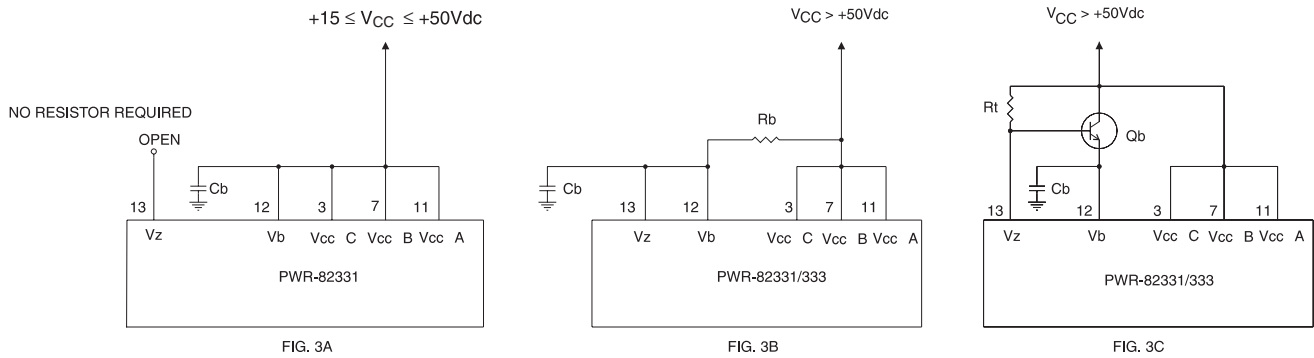
If the system bus voltage is greater than +50 Vdc (and a lower voltage is not available), then the  $V_b$  pin and  $V_z$  pin can be tied together with an external power resistor ( $R_b$ ) and connected from these pins to the system power bus. (See FIGURE 3B).

See FIGURES 4 and 5 for bias resistor characteristics.

If additional power dissipation in  $R_b$  is a concern, FIGURE 3C shows a more efficient design, using a low-power resistor ( $R_t$ ) and an additional transistor. To determine the proper resistor to use, refer to FIGURE 6.

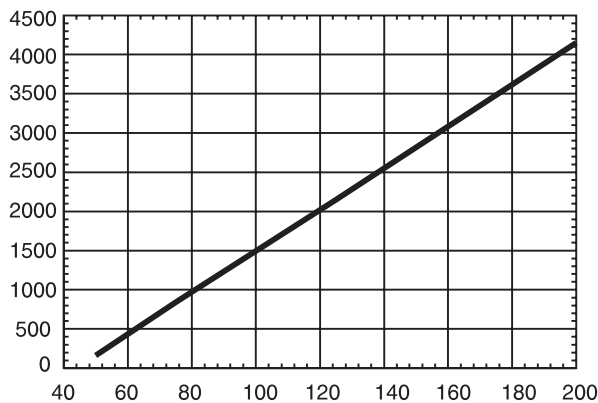
If there is another voltage available in the system in the +15 to +50 Vdc range, then this voltage can be directly connected to the  $V_b$  pin of the hybrid.

**In any case, a 0.01 mF decoupling capacitor ( $C_b$ ) must be connected between  $V_b$  (pin 12) and GND.**

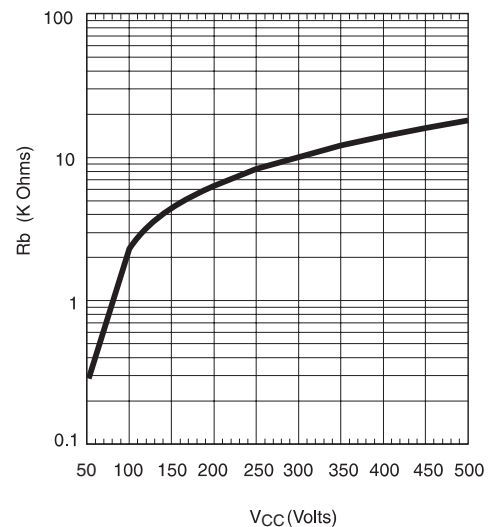


NOTE:  $C_b = 0.01\text{mF}$ , 100V, CERAMIC; FOR PWR-82331,  $Q_b = 200\text{V}$ , 6W TRANSISTOR; FOR PWR-82333,  $Q_b = 500\text{V}$ , 12W TRANSISTOR

**FIGURE 3. CONNECTION TO BUS VOLTAGE TO DEVELOP PROPER INPUT BIAS VOLTAGE**



**FIGURE 4A. PWR-82331**



**FIGURE 4B. PWR-82333**

**FIGURE 4. BIAS RESISTOR VALUE ( $R_b$ ) VS. BUS VOLTAGE ( $V_{CC}$ )**

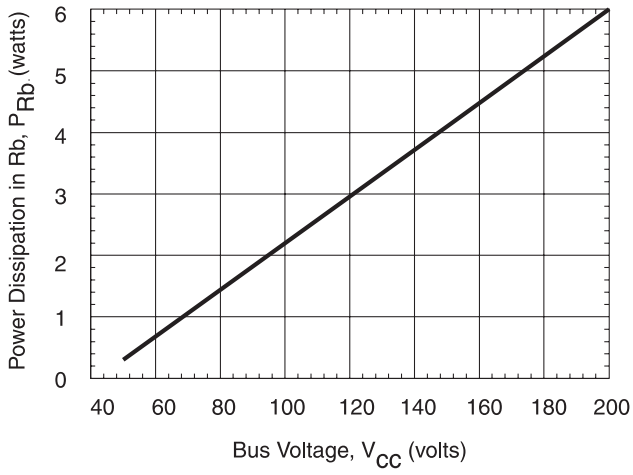


FIGURE 5A. PWR-82331

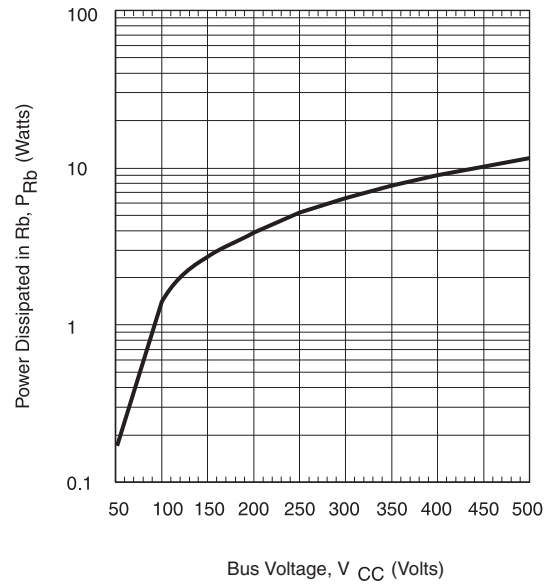


FIGURE 5B. PWR-82333

FIGURE 5. POWER DISSIPATED IN BIAS RESISTOR ( $R_b$ ) VS. BUS VOLTAGE ( $V_{CC}$ )

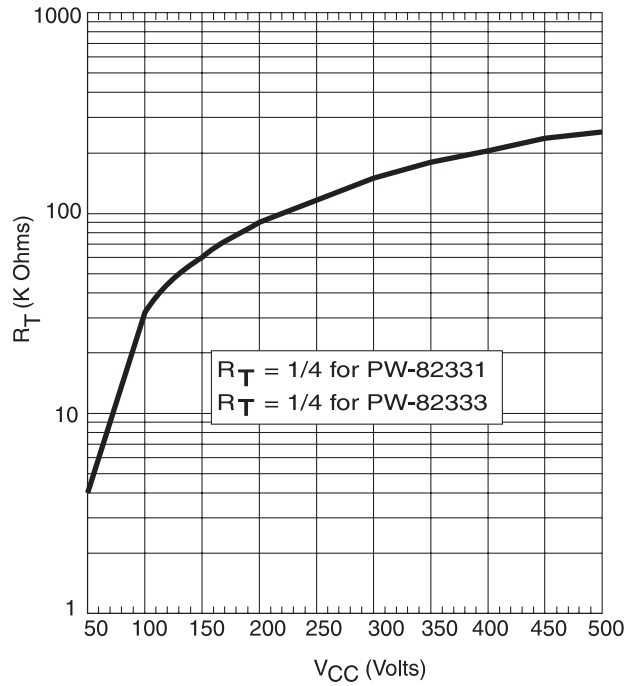


FIGURE 6.  $R_T$  RESISTOR VALUE VS. BUS VOLTAGE

## DIGITALLY CONTROLLED INPUTS

The PWR-82331/82333 uses Schmitt triggered digital inputs (with hysteresis) to ensure high-noise immunity. The trigger switches at different points for positive and negative going signals. The hysteresis voltage ( $V_H$ ) is the difference between the positive going voltage ( $V_P$ ) and the negative going voltage ( $V_N$ ) (see FIGURE 7). The digital inputs have programmable logic levels, which allows the hybrid to be used with different types of commutation logic with an input voltage range of +5 V to +15 V, such as TTL or CMOS logic. The PWR-82331/82333 internal power supply generates a +15 Vdc ( $V_{LPO}$ ) on pin 15. This output can only be used to power the internal digital circuitry within the hybrid. **Do not use this +15 V output to power any circuitry external to the hybrid.** Pin 16 is the logic power input ( $V_{LPI}$ ) for the digital circuitry inside the hybrid. **A 0.01 mF, +50 V ceramic capacitor must be placed between this pin (16) and GND as close to the hybrid as possible.** When using +15 V control circuitry, the logic power input (pin 16) can be connected directly to logic power output (pin 15) of the hybrid. There is no need for an additional external power supply.

When using +5 V control logic, an external +5 Vdc supply must be connected between pin 16 of the hybrid and the GND - leave Pin 15 open (N/C). The commutation/control circuitry can be as simple as discrete logic with PWM, or as sophisticated as a microprocessor or custom ASIC, depending on the system requirements. The block diagram in FIGURE 8 shows a typical interface of the PWR-82331/82333 with a motor and commutation logic in a servo-amp system.

## INTERFACING WITH OPTOCOUPLERS

Optocouplers should be used when the commutation logic cannot be located directly next to the motor drive (within 1"- 2" from the input) or a current sensing resistor is placed between VSS and POWER RTN (see FIGURE 9). The optocouplers minimize the differential ground voltage drop between the logic grounds and the VSS connections. Optocouplers are also required when +5 V logic is used to control the motor drive.

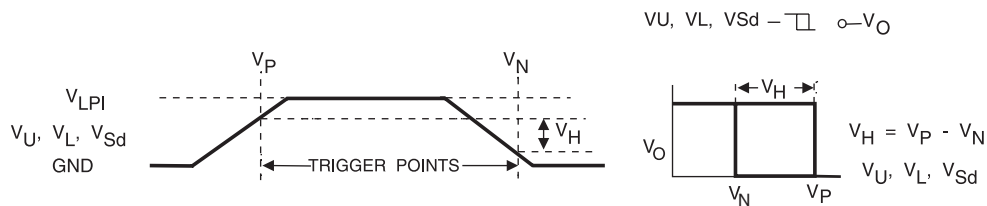


FIGURE 7. HYSTERESIS DEFINITION AND CHARACTERISTICS

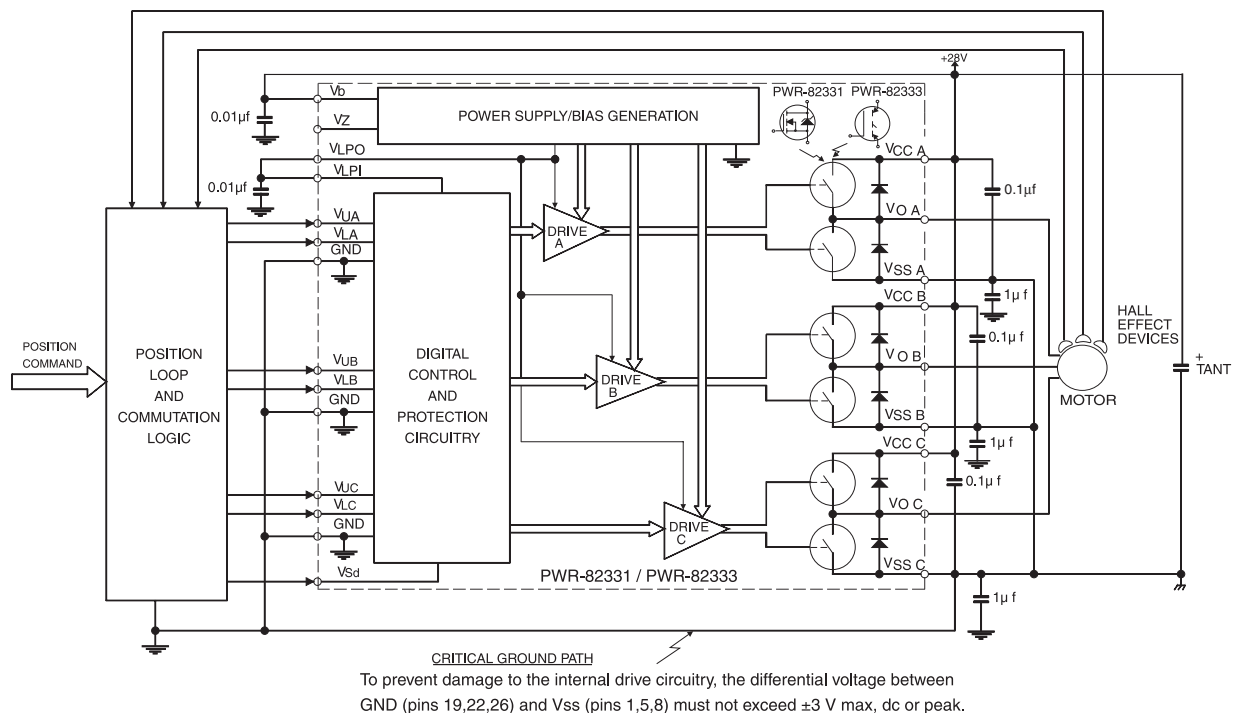


FIGURE 8. PWR-82331/82333 TYPICAL INTERFACE WITH A MOTOR AND COMMUTATION LOGIC

## SHUT-DOWN INPUT (VSD)

Pin 23 (Vsd) provides a digital shut-down input, which allows the user to completely turn-off both the upper and lower output transistors in all 3-phases. Application of a logic “1” to the Vsd input will latch the Digital Control/Protection circuitry thereby turning off all output transistors. The Digital Control/Protection circuitry remains latched in the off-state and will not respond to signals on the VL or VU inputs while the Vsd has a logic “1” applied. When the user or the sense circuitry (as in FIGURE 9) returns the Vsd input to a logic “0,” and then the user sets the VL and VU inputs to a logic “0” the output of the Digital Control/Protection circuitry will clear the internal latch. When the next rising edge (see FIGURE 10) occurs on the VL or VU digital inputs, the output transistors will respond to the corresponding digital input. This feature can be used with external current limit or temperature sense circuitry to disable the drive if a fault condition occurs.

## INTERNAL PROTECTION CIRCUITRY

The hybrid contains digital protection circuitry, which prevents in-line transistors from conducting simultaneously. This, in effect, would short circuit the power supply and would damage the output stage of the hybrid. The circuitry allows only proper input signal patterns to cause output conduction. FIGURE 10 and TABLE 3 show these timing relationships. If an improper input requested that the upper and lower transistors of the same phase conduct together, the output would be a high impedance until removal of the illegal code from the input of the PWR-82331/82333. A dead time of 500 ns minimum should still be maintained between the signals at the VU and VL pins; this ensures the complete turn off of any transistor before turning on its associated in-line transistor.

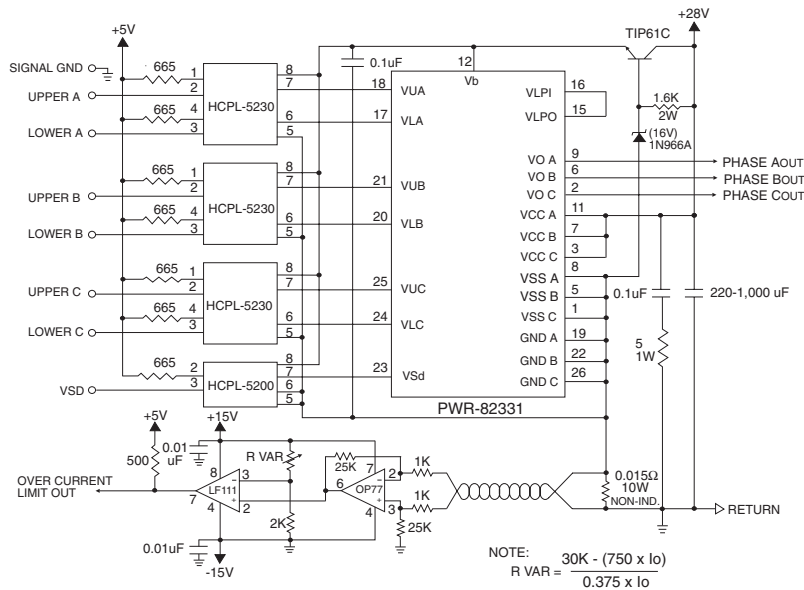


FIGURE 9. TYPICAL OPTOCOUPLER APPLICATION

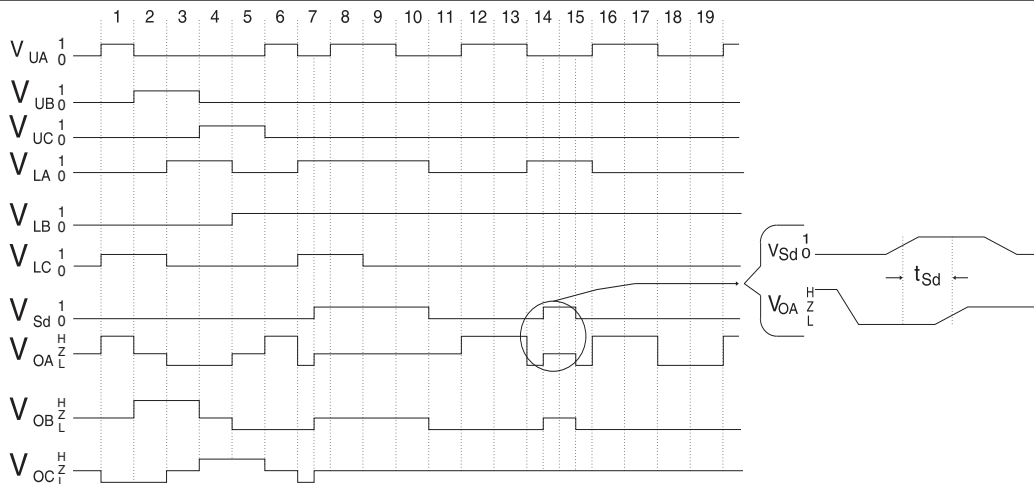


FIGURE 10. SHUT-DOWN (Vsd) TIMING RELATIONSHIPS



## PWR-82331 POWER DISSIPATION (SEE FIGURE 11)

There are three major contributors to power dissipation in the motor driver: conduction losses, switching losses, and flyback diode losses.

VCC = +140 V (Bus Voltage)

IOA = 20 A (See FIGURE 11); IOB = 30 A; (See FIGURE 11)

ton = 20 μs (See FIGURE 11); T = 40 μs (period)

Ron = 0.1 Ω (on-resistance see TABLE 2, IO = 30 A, TC = +25° C)

ts1 = 250 ns (see FIGURE 11); ts2 = 250 ns (see FIGURE 11)

fo = 25 kHz (switching frequency)

VF is the diode forward voltage, Table 2, IO = 30 A, TC = +25° C

VF(avg) = +1.15 V; IF is the diode forward current

### 1. Conduction Losses (Pc)

$$P_c = (I_{\text{motor rms}})^2 \times R_{\text{on}}$$

$$I_{\text{motor rms}} = \sqrt{\left( I_{\text{OB}}^2 - I_{\text{OB}}(I_{\text{OB}} - I_{\text{OA}}) + \frac{(I_{\text{OB}} - I_{\text{OA}})^2}{3} \right) \left( \frac{t_{\text{on}}}{T} \right)}$$

$$I_{\text{motor rms}} = \sqrt{\left( 30^2 - 30(30 - 20) + \frac{(30 - 20)^2}{3} \right) \left( \frac{20}{40} \right)}$$

$$P_c = (17.80 \text{ A})^2 \times (0.1 \Omega)$$

$$P_c = 31.68 \text{ Watts}$$

### 2. Switching Losses (Ps)

$$P_s = [V_{\text{CC}}(I_{\text{OA}}(t_{\text{s1}}) + I_{\text{OB}}(t_{\text{s2}})) f_o] / 2$$

$$P_s = [140(20(250 \text{ ns}) + 30(250 \text{ ns}))25\text{k}] / 2$$

$$P_s = 21.88 \text{ Watts}$$

### 3. Flyback Diode Losses (Pdf)

$$P_{\text{df}} = I_{\text{F}}(\text{avg}) \times V_{\text{F}}(\text{avg})$$

$$I_{\text{F}}(\text{avg}) = [(I_{\text{OB}} + I_{\text{OA}}) / 2] / 2 = [(30 + 20) / 2] / 2 = 12.5 \text{ A}$$

$$P_{\text{df}} = 12.5 \text{ A} \times 1.15 \text{ V}$$

$$P_{\text{df}} = 14.38 \text{ Watts}$$

### Transistor Power Dissipation (PQ)

To calculate the maximum power dissipation of the output transistor as a function of the case temperature use the following equation. (Reference FIGURE 20 to ensure you don't exceed the maximum allowable power dissipation of each transistor.)

$$P_Q = P_c + P_s$$

### Total Hybrid Power Dissipation (PTOTAL)

To calculate Total Power dissipated in the hybrid use:

$$P_{\text{TOTAL}} = \sum_{i=1}^6 [P_{\text{Qi}} + P_{\text{difi}}] \text{ where } i = \text{each transistor or diode.}$$

## PWR-82333 POWER DISSIPATION (SEE FIGURE 11)

There are three major contributors to power dissipation in the motor driver: conduction losses, switching losses, and flyback diode losses.

VCC = +270 V (Bus Voltage)

IOA = 20 A (See FIGURE 11); IOB = 30 A; (See FIGURE 11)

ton = 50 μs (See FIGURE 11); T = 100 μs (period)

VCE(SAT) = 3.8 V (see TABLE 2, IO = 30 A, TC = +25° C)

ts1 = 300 ns (see FIGURE 11); ts2 = 300 ns (see FIGURE 11)

fo = 10 kHz (switching frequency)

VF is the diode forward voltage, TABLE 2, IO = 30 A, TC = +25° C

VF (avg) = +1.70 V; IF is the diode forward current

### 1. Conduction Losses (Pc)

$$P_c = (I_{\text{motor rms}}) \times V_{\text{CE(SAT)}}$$

$$I_{\text{motor rms}} = \sqrt{\left( I_{\text{OB}}^2 - I_{\text{OB}}(I_{\text{OB}} - I_{\text{OA}}) + \frac{(I_{\text{OB}} - I_{\text{OA}})^2}{3} \right) \left( \frac{t_{\text{on}}}{T} \right)}$$

$$I_{\text{motor rms}} = \sqrt{\left( 30^2 - 30(30 - 20) + \frac{(30 - 20)^2}{3} \right) \left( \frac{50}{100} \right)}$$

$$P_c = (17.80 \text{ A}) \times (3.8 \text{ V})$$

$$P_c = 67.64 \text{ Watts}$$

### 2. Switching Losses (Ps)

$$P_s = [V_{\text{CC}}(I_{\text{OA}}(t_{\text{s1}}) + I_{\text{OB}}(t_{\text{s2}})) f_o] / 2$$

$$P_s = [270(20(300 \text{ ns}) + 30(300 \text{ ns}))10\text{k}] / 2$$

$$P_s = 20.25 \text{ Watts}$$

### 3. Flyback Diode Losses (Pdf)

$$P_{\text{df}} = I_{\text{F}}(\text{avg}) \times V_{\text{F}}(\text{avg})$$

$$I_{\text{F}}(\text{avg}) = [(I_{\text{OB}} + I_{\text{OA}}) / 2] / 2 = [(30 + 20) / 2] / 2 = 12.5 \text{ A}$$

$$P_{\text{df}} = 12.5 \text{ A} \times 1.70 \text{ V}$$

$$P_{\text{df}} = 21.25 \text{ Watts}$$

### Transistor Power Dissipation (PQ)

To calculate the maximum power dissipation of the output transistor as a function of the case temperature use the following equation. (Reference FIGURE 20 to ensure you don't exceed the maximum allowable power dissipation of each transistor.)

$$P_Q = P_c + P_s$$

### Total Hybrid Power Dissipation (PTOTAL)

To calculate Total Power dissipated in the hybrid use:

$$P_{\text{TOTAL}} = \sum_{i=1}^6 [P_{\text{Qi}} + P_{\text{difi}}] \text{ where } i = \text{each transistor or diode.}$$

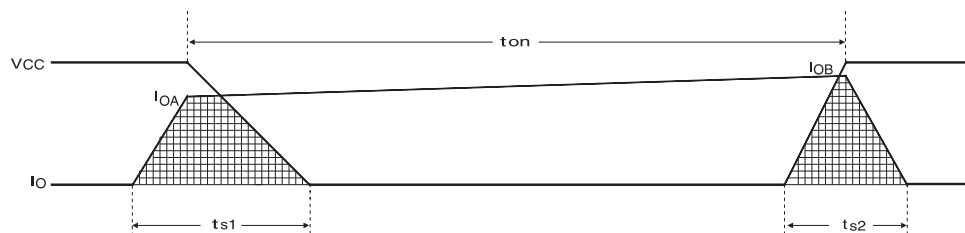


FIGURE 11. OUTPUT CHARACTERISTICS

## GROUND CONNECTIONS

### LAYOUT AND EXTERNAL COMPONENTS

**Important:** The following layout guidelines and required external components are critical to the proper operation of these motor drives.

External connections can be easily made to the hybrid by any of the following methods:

- Solder a wire around each pin.
- Use pin extenders to raise the height of each pin so a printed circuit board can be mounted on top of the hybrid.
- Use a printed circuit board with a cutout that will enable the printed circuit board to slide over the pins.

**Permanent damage will result to the motor drive if the user does not make the following recommended ground connections that will ensure the proper orientation of the hybrid.**

The Vb and logic grounds are on pins 19, 22 and 26 (GND). The VSS connections for the output stage are on pins 1, 5, and 8 (VSS). **To prevent damage to the internal drive circuitry, the differential voltage between the GND (pins 19, 22, 26) and VSS (pins 1, 5, 8) must not exceed  $\pm 3$  V max, dc or peak.** This includes the combined voltage drop of the associated

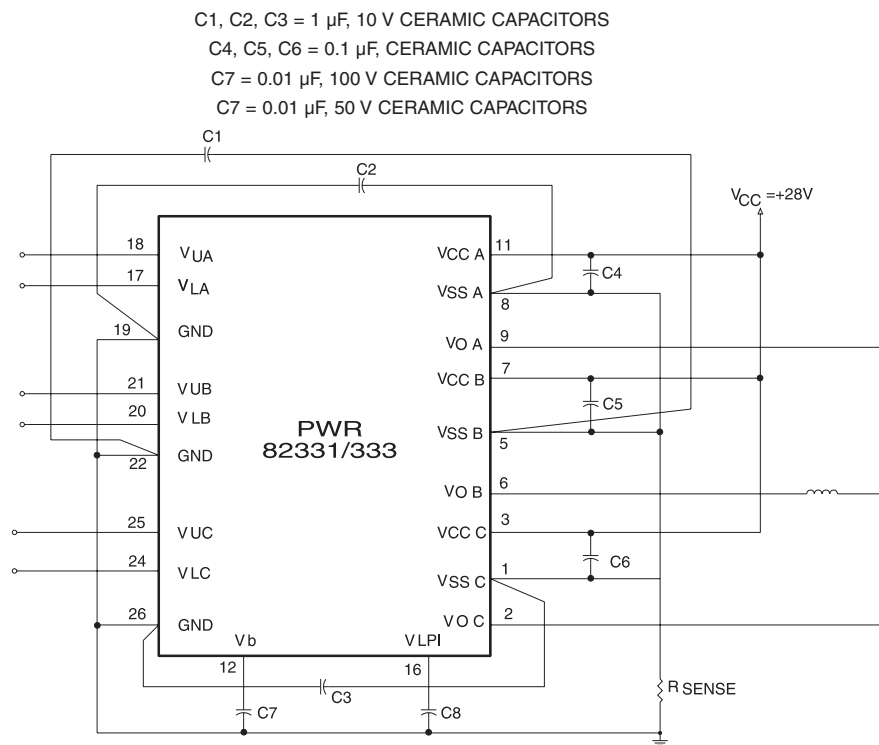
ground paths and the voltage drop across RSENSE (see FIGURE 12).

For example, a value for RSENSE of  $0.025 \Omega$  will give a voltage drop of +1.25 V at 50 A and allow enough margin for the voltage drop in the ground conductors. Locate RSENSE 1" - 2" maximum from the hybrid. It is critical that all ground connections be as short, and of lowest impedance, as the system allows.

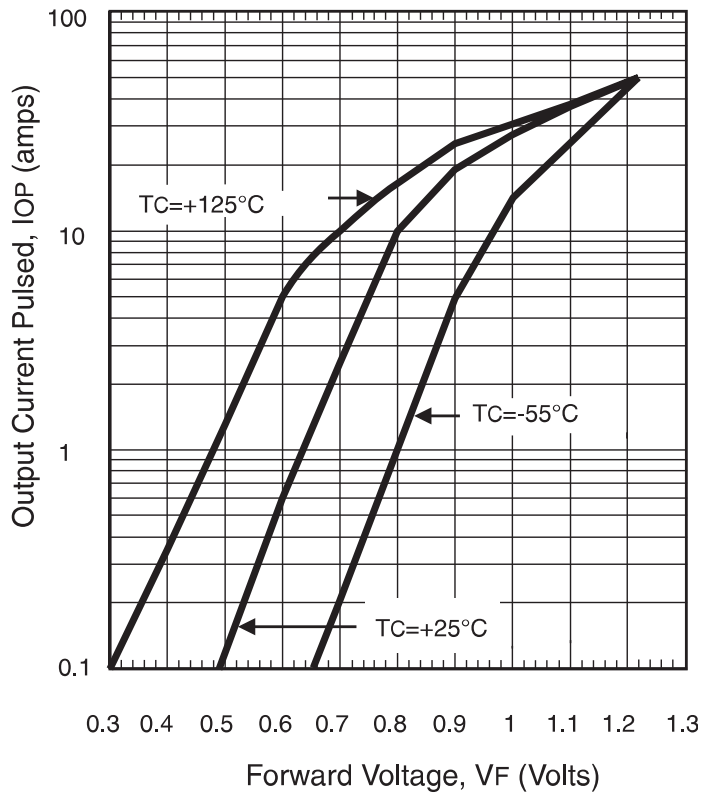
C1, C2, and C3 are 1 mF, +10 V ceramic capacitors that provide a low ac impedance between Vss pin and GND. You must use one capacitor for each VSS pin-to-GND connection (total of three capacitors in all), these capacitors are independent of the type of drive scheme used. (i.e., Trapezoidal or Sinusoidal drive). Since placement of these capacitors is critical, place these capacitors across the hybrid, if possible. Please note, on FIGURE 12, that C1, C2, and C3 must go directly from terminal-to-terminal on the hybrid - do not daisy chain along the ground return.

C4, C5, and C6 are the 0.1 mF ceramic bypass capacitors that suppress high frequency spiking. The voltage rating should be two times the maximum system voltage. These capacitors should be located as close to the hybrid as possible.

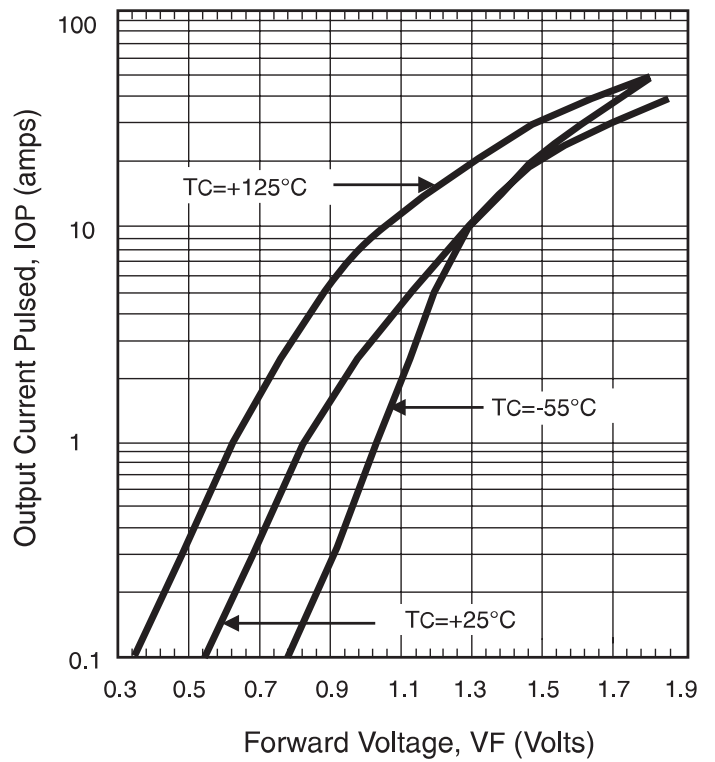
Care must be taken to control the regenerative energy produced by the motor in order to prevent excessive spiking on the Vcc line. Accomplish this by placing a capacitor or clamping diode between the Vcc and the high-power ground return.



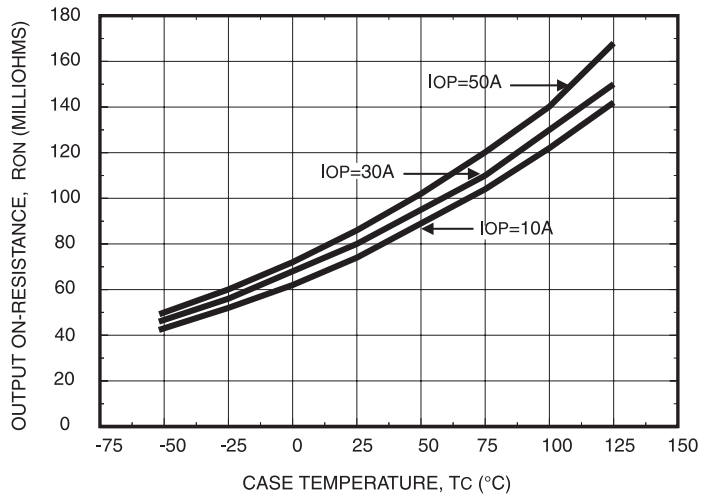
**FIGURE 12. PWR-82331/82333 GROUND CONNECTIONS**



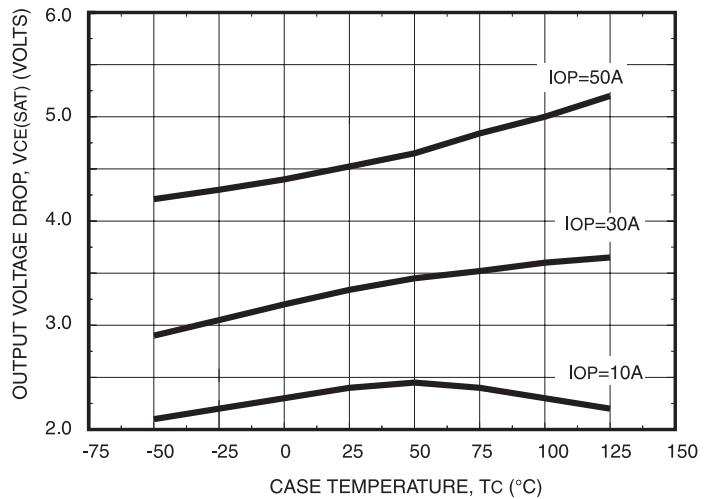
**FIGURE 13A. PWR-82331 TYPICAL FORWARD VOLTAGE DROP OF FLYBACK DIODES**



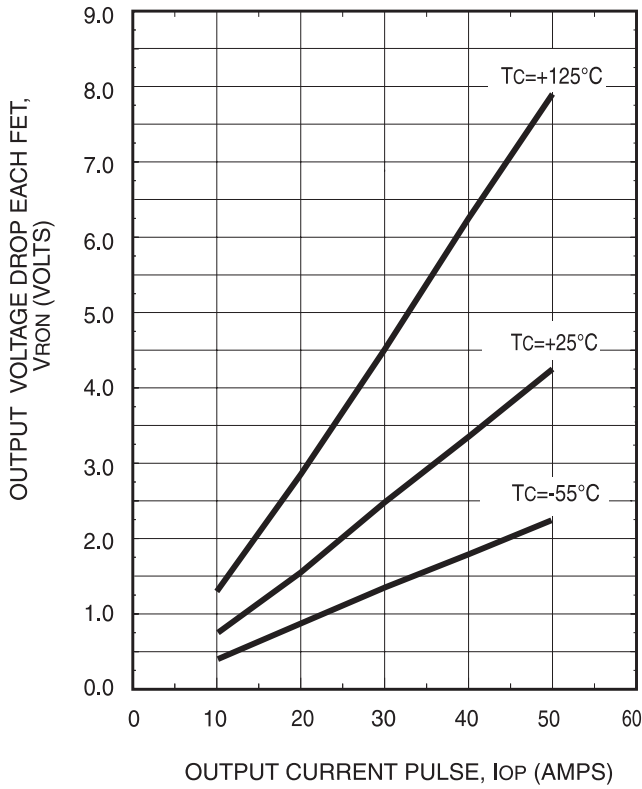
**FIGURE 13B. PWR-82333 TYPICAL FORWARD VOLTAGE DROP OF FLYBACK DIODES**



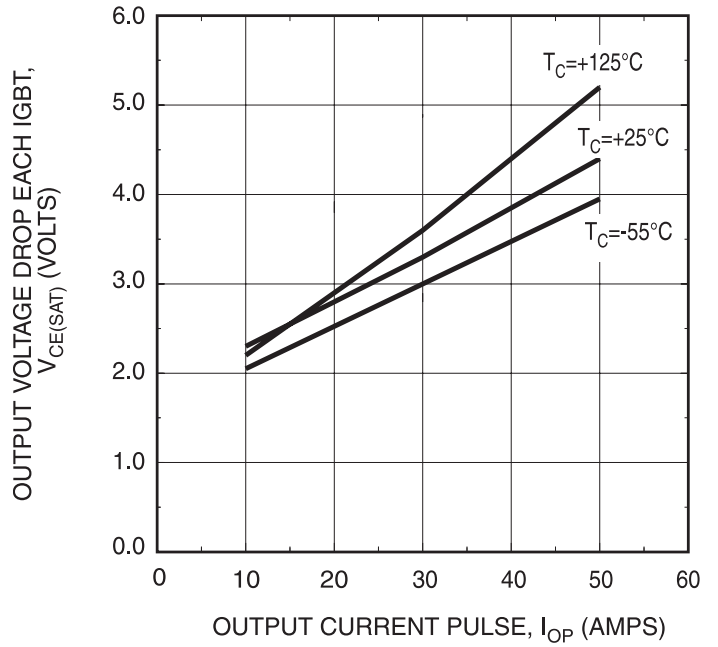
**FIGURE 14A. PWR-82331 TYPICAL ON RESISTANCE VARIATION WITH TEMPERATURE**



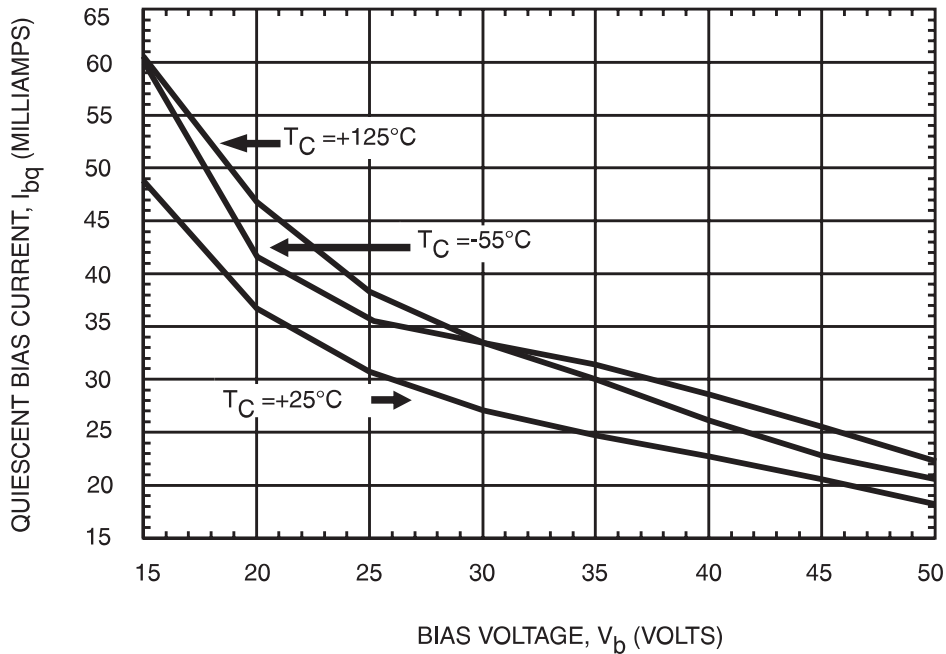
**FIGURE 14B. PWR-82333 TYPICAL V<sub>CE(SAT)</sub> VARIATION WITH TEMPERATURE**



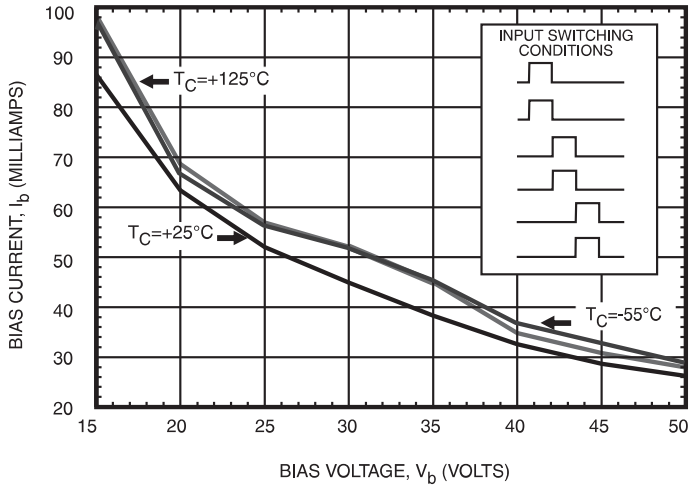
**FIGURE 15A. PWR-82331 TYPICAL OUTPUT ON VOLTAGE DROP VERSUS OUTPUT CURRENT**



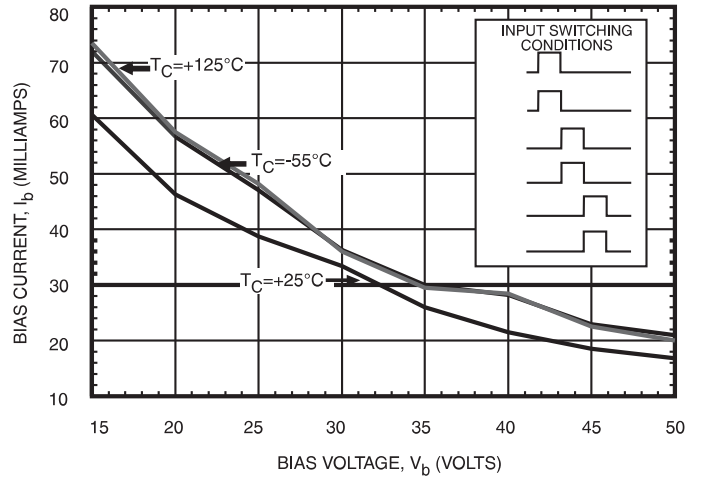
**FIGURE 15B. PWR-82333 TYPICAL OUTPUT ON VOLTAGE VERSUS OUTPUT CURRENT**



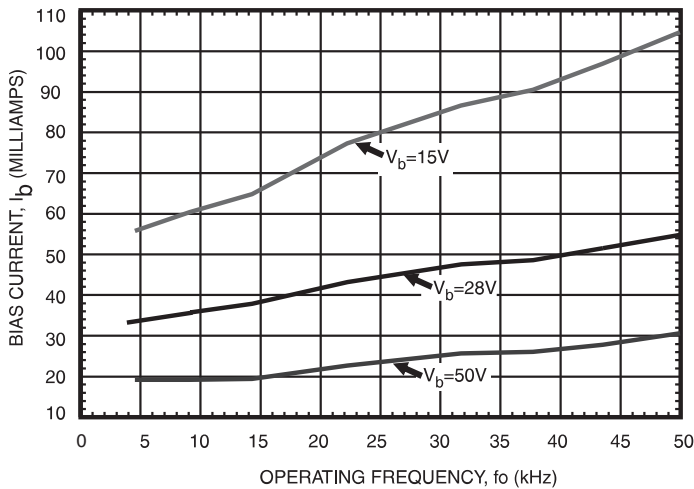
**FIGURE 16. PWR-82331/82333 TYPICAL QUIESCENT BIAS CURRENT VERSUS BIAS VOLTAGE**



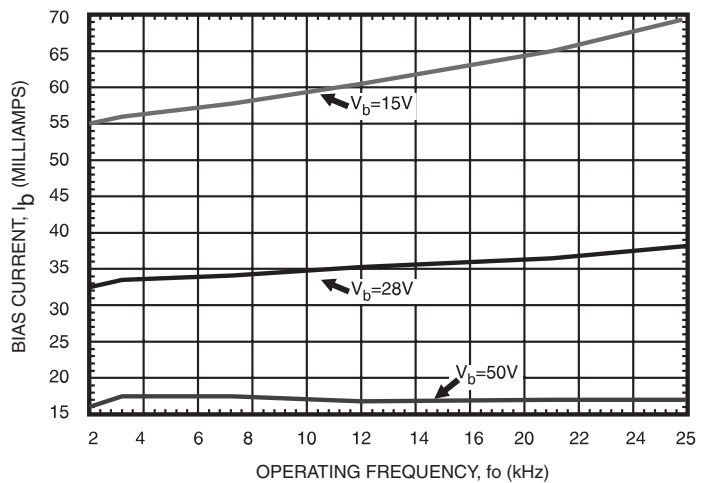
**FIGURE 17A. PWR-82331 TYPICAL BIAS CURRENT VERSUS BIAS VOLTAGE AT  $f_o = 30$  kHz**



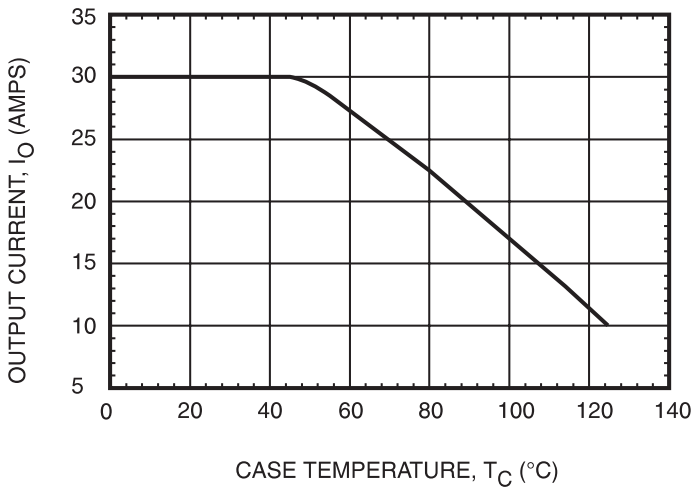
**FIGURE 17B. PWR-82333 TYPICAL BIAS CURRENT VERSUS BIAS VOLTAGE AT  $f_o = 10$  kHz**



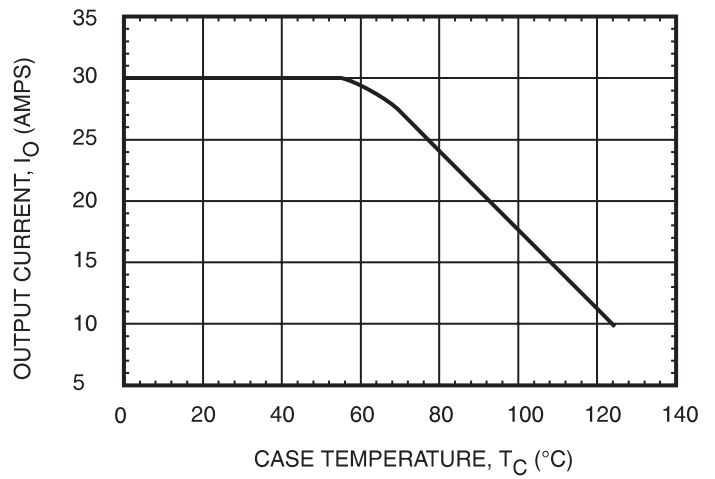
**FIGURE 18A. PWR-82331 BIAS CURRENT VERSUS OPERATING FREQUENCY**



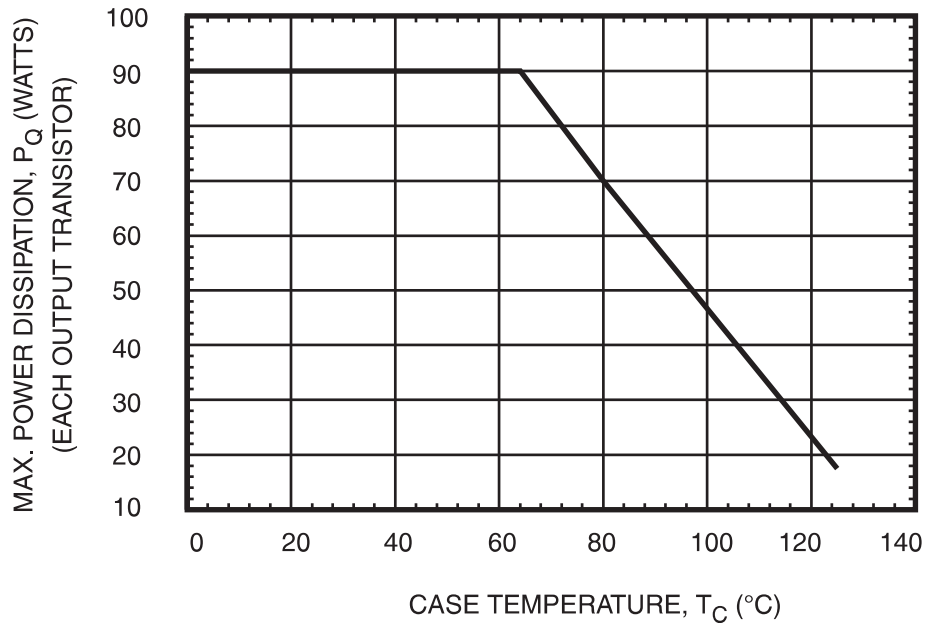
**FIGURE 18B. PWR-82333 BIAS CURRENT VERSUS OPERATING FREQUENCY**



**FIGURE 19A. PWR-82331  
MAXIMUM ALLOWABLE CONTINUOUS OUTPUT  
CURRENT VERSUS CASE TEMPERATURE**



**FIGURE 19B. PWR-82333  
MAXIMUM ALLOWABLE CONTINUOUS OUTPUT  
CURRENT VERSUS CASE TEMPERATURE**



**FIGURE 20. PWR-82331/82333  
MAXIMUM ALLOWABLE POWER DISSIPATION OF EACH OUTPUT TRANSISTOR  
VERSUS CASE TEMPERATURE**

**TABLE 3. INPUT-OUTPUT TRUTH TABLE**

INPUTS							OUTPUTS		
UPPERS			LOWERS			CONTROL	Vo A	Vo B	Vo C
VUA	VUB	VUC	VLA	VLB	VLC	Vsd			
1	0	0	0	1	0	0	H	L	Z
1	0	0	0	0	1	0	H	Z	L
0	1	0	0	0	1	0	Z	H	L
0	1	0	1	0	0	0	L	H	Z
0	0	1	1	0	0	0	L	Z	H
0	0	1	0	1	0	0	Z	L	H
0	0	1	1	1	0	0	L	L	H
0	1	0	1	0	1	0	L	H	L
0	1	1	1	0	0	0	L	H	H
1	0	0	0	1	1	0	H	L	L
1	0	1	0	1	0	0	H	L	H
1	1	0	0	0	1	0	H	H	L
0	1	1	1	0	1	0	L	H	Z
0	1	1	1	1	0	0	L	Z	H
1	0	1	0	1	1	0	H	L	Z
1	0	1	1	1	0	0	Z	L	H
1	1	0	0	1	1	0	H	Z	L
0	0	0	0	0	0	0	Z	Z	Z
0	0	0	1	1	1	0	L	L	L
1	1	1	0	0	0	0	H	H	H
x	x	x	x	x	x	1	Z	Z	Z

H = High Level, L = Low Level, X = Irrelevant, Z = High Impedance

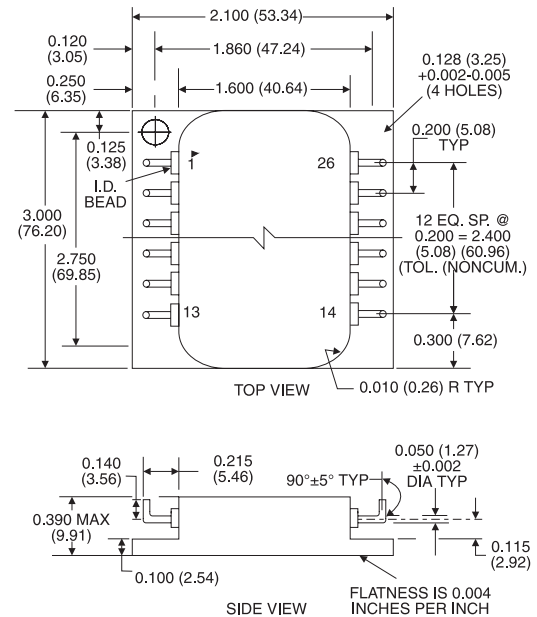
**TABLE 4. PIN ASSIGNMENTS**

PIN	FUNCTION	PIN	FUNCTION
1	VSS C	26	GND
2	Vo C	25	VUC
3	VCC C	24	VLC
4	N/C	23	Vsd
5	VSS B	22	GND
6	Vo B	21	VUB
7	VCC B	20	VLB
8	VSS A	19	GND
9	Vo A	18	VUA
10	N/C	17	VLA
11	VCC A	16	VLPI
12	Vb	15	VLPO
13	Vz	14	N/C

Notes: 1. Pins 3, 7, and 11 are internally connected.  
 2. Pins 19, 22 and 26 are internally connected.

**MOUNTING**

The package bolts to part of the chassis or even the motor assembly itself, depending on system requirements. In applications where this isn't convenient, the hybrid can be mounted to its own heatsink. The heat transfer in the hybrid is from semiconductor junction to the bottom of the hybrid case. The flatness and maximum temperature of this mounting surface are critical to proper performance and reliability, because this is the only method of dissipating the power created in the hybrid. Use a mounting surface flatness of 0.004 inches/inch maximum. This interface can be improved with the use of a thermal compound or pad. The heatsink should be designed to insure that the case temperature does not exceed +125°C.



**FIGURE 21. PWR-82331/82333 MECHANICAL OUTLINE**

## ORDERING INFORMATION

PWR-8233X-XX0X

### Supplemental Process Requirements:

S = Pre-Cap Source Inspection  
 L = 100% Pull Test  
 Q = 100% Pull Test and Pre-Cap Source Inspection  
 Blank = None of the Above

### Process Requirements:

0 = Standard DDC Processing, no Burn-In (See table below.)  
 1 = MIL-PRF-38534 Compliant \*\*  
 2 = B\*  
 3 = MIL-PRF-38534 Compliant with PIND Testing \*\*  
 6 = B\* with PIND Testing

### Temperature Grade/Data Requirements:

1 = -55°C to +125°C  
 2 = -40°C to +85°C  
 3 = 0°C to +70°C  
 4 = -55°C to +125°C with Variables Test Data  
 5 = -40°C to +85°C with Variables Test Data  
 8 = 0°C to +70°C with Variables Test Data

### Rating:

1 = 200 V using MOSFETs  
 3 = 500 V using IGBTs

\*Standard DDC Processing with burn-in and full temperature test — see table below.

\*\* Contact factory for availability.

STANDARD DDC PROCESSING FOR HYBRID AND MONOLITHIC HERMETIC PRODUCTS		
TEST	MIL-STD-883	
	METHOD(S)	CONDITION(S)
INSPECTION	2009, 2010, 2017, and 2032	—
SEAL	1014	A and C
TEMPERATURE CYCLE	1010	C
CONSTANT ACCELERATION	2001	3000g
BURN-IN	1015 (note 1), 1030 (note 2)	TABLE 1

Notes:

1. For Process Requirement "B\*" (refer to ordering information), devices may be non-compliant with MIL-STD-883, Test Method 1015, Paragraph 3.2. Contact factory for details.

2. When applicable.



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Specifications are subject to change without notice.

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**France** - Tel: +33-(0)1-41-16-3424, Fax: +33-(0)1-41-16-3425

**Germany** - Tel: +49-(0)89-150012-11, Fax: +49-(0)89-150012-22

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