

5.5V to 28V Input, 2ch Synchronous Buck DC/DC Controller

BD9528AMUV

General Description

BD9528AMUV is a dual buck regulator controller with adjustable output voltage from1.0V to 5.5V and an input voltage range of 5.5 to 28V. High efficiency is achieved with an external synchronous Nch-MOSFET. H³Reg[™], Rohm's advanced proprietary control method that uses constant on-time control to provide ultra high transient responses to load changes is used. SLLM(Simple Light Load Mode) technology is added to improve efficiency with light loads giving high efficiency over a wide load range. In addition to the dual buck regulator controllers, here are 2 LDO regulators included that are fixed output voltage of 3.3V and 5.0V. Other functions included are soft start, variable frequency, short circuit protection with timer latch, over voltage, and power good outputs. This buck regulator is optimal for high-current applications.

Features

- Adjustable Simple Light Load Mode (SLLM), Quiet light Load Mode (QLLM), Forced continuous Mode.
- Multifunctional Protection Circuit

 Settable Over Current Protection (OCP)
 Thermal Shut down (TSD)
 Under Voltage Lock Out (UVLO)
 Over Voltage Protection (OVP)
 Short Circuit Protection with Timer-Latch (SCP)
- 150kHz to 500kHz Switching frequency.
- Adjustable Soft Start.
- Power Good.
- Dual Linear Regulator (5V/3.3V (total 100mA)).
- Output Discharge.
- Reference voltage Circuit (0.7V).
- Boot diode

Applications

 Industrial Equipment ,FPGA, POL Power Supply, Mobile PC, Desktop PC, LCD-TV, Digital Components, etc.

Key Specifications

- Input Voltage Range: 5.5V to 28V
 - Output Voltage Range: 1.0V to 5.5V
- Switching Frequency: 200k to 500kHz(Typ)
- Operating Temperature Range: -20°C to +100°C

Package

VQFN032V5050

W(Typ) x D(Typ) x H(Max) 5.00mm x 5.00mm x 1.00mm



BD9528AMUV

Typical Application Circuit

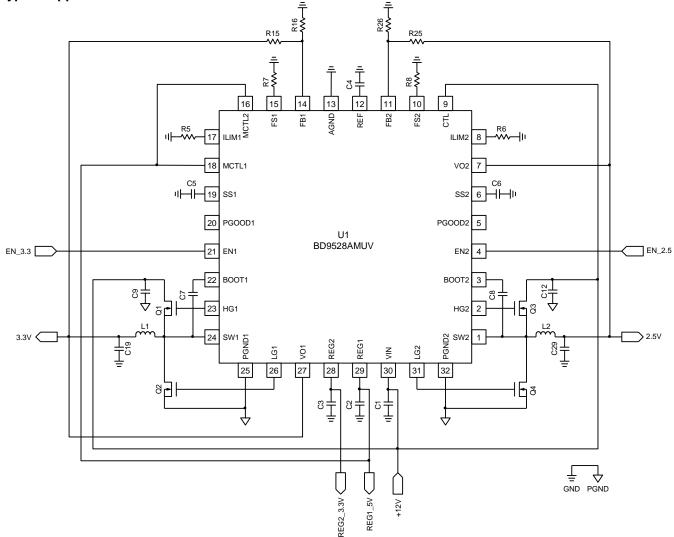


Figure 1. Application Circuit

Pin Configuration

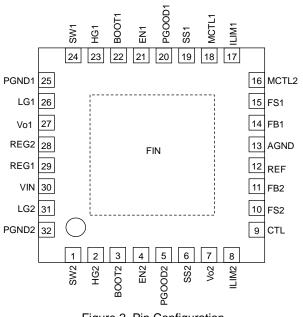


Figure 2. Pin Configuration

Pin Descriptions

Pin No.	Pin Name	Function							
1 24	SW2 SW1	Ground pin for High-side FET. The maximum voltage range of this pin is 30V.							
2 23	HG2 HG1	High-side FET gate drive pin.							
3 22	BOOT2 BOOT1	ground is to 35V, to	This is the power supply pin for High-side FET driver. The maximum voltage range to ground is to 35V, to SW pin is to 7V. In switching operations, the voltage swings from (VIN+REG1) to REG1 by BOOT pin operation.						
4 21	EN2 EN1		atus switches o	off when EN p	s of the switching regulator be in voltage goes lower than 0.8 istor.				
5 20	PGOOD2 PGOOD1				oltage, it will output low level. nnect pull-up resistance.				
6 19	SS2 SS1	between SS and g	This is the setting pin for soft start. The rising time is determined by the capacitor connected between SS and ground, and the fixed current inside IC after it is the status of low in standby mode. It controls the output voltage till SS voltage catch up the REF pin to become the SS						
7 27	VO2 VO1	This is the output c	lischarge pin,	and output vo	Itage feedback pin for frequer	ncy setting.			
8 17	ILIM2 ILIM1	This is the coil curr	ent limit settin	g pin. Set the	resistor which is connected ir	n between ground.			
9	CTL	When CTL pin voltage is at least 2.3V, the status of the linear regulator REG1 and REG2 output becomes active. Conversely, the status switches off when CTL pin voltage goes lower than 0.8V. The switching regulator doesn't become active when the status of CTL pin is low, if the status of EN pin is high. This pin is pulled up to VIN with $1M\Omega$ resistor.							
10 15	FS2 FS1	Frequency input. A resistor to ground will set the switching frequency. Frequencies from 150kHz to 500kHz are possible.							
11 14	FB2 FB1	This is the output v The IC controls ref	This is the output voltage feedback pin. The IC controls reference voltage and FB terminal voltage are almost same.						
12	REF	This is the output voltage setting pin. The IC controls reference voltage and FB terminal voltage are almost same.							
13	AGND	Ground input for co	_						
16	MCTL2	Level.	reaches more	•	nal voltage reaches less than will be High Level. This pin is Control Mode				
18	MCTL1		Low	Low	SLLM				
			Low	High	QLLM	-			
			High	Low	Continuous PWM Mode				
			High	High	Continuous PWM Mode				
25 32	PGND1 PGND2	This is the ground	pin for Low-si	de FET drive.		-			
26 31	LG1 LG2	ON resistance of o	This is the Low-side FET gate drive pin. It is operated in switching between REG1 to PGND. ON resistance of output stage when High, it is 2Ω and when Low, it is 0.5Ω drive Low-side FET gate with the high pace.						
28	REG2	This is the output p	This is the output pin for 3.3V/50mA linear regulator (5V/3.3V (total 100mA)). Please connect 10µF capacitor which characteristic is more than X5R near the pin.						
29	REG1				ator (5V/3.3V (total 100mA)). eristic is more than X5R near	the pin.			
30	VIN	necessary on-time	. As a result, t	his terminal v	r regulator. Monitor input volta oltage changes, and then the citor which characteristic is mo	IC operation			
FIN	FIN	This is the thermal	PAD. Please	connect to the	e ground.				

Output condition table

Input			Output				
CTL	EN1	EN2	REG1(5V)	REG2(3.3V)	DC/DC1	DC/DC2	
Low	Low	Low	OFF	OFF	OFF	OFF	
Low	Low	High	OFF	OFF	OFF	OFF	
Low	High	Low	OFF	OFF	OFF	OFF	
Low	High	High	OFF	OFF	OFF	OFF	
High	Low	Low	ON	ON	OFF	OFF	
High	Low	High	ON	ON	OFF	ON	
High	High	Low	ON	ON	ON	OFF	
High	High	High	ON	ON	ON	ON	

* CTL pin is connected to VIN pin with $1M\Omega$ resistor(pull up) internal IC. * EN pin is connected to AGND pin with $1M\Omega$ resistor(pull down) internal IC.

Block Diagram

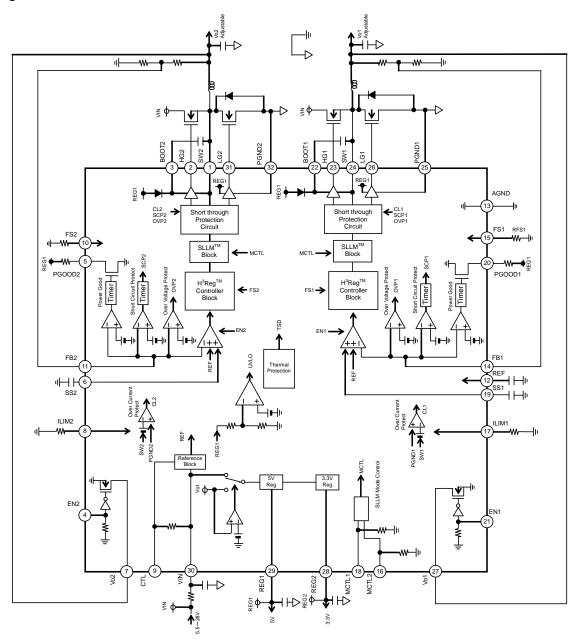


Figure 3. Block Diagram

Absolute Maximum Ratings(Ta = 25°C)

Parameter	Symbol	Rating	Unit	Conditions
	VIN, CTL, SW1, SW2	30	V	Note 1
	EN1, EN2, PGOOD1, PGOOD2 Vo1, Vo2, MCTL1, MCTL2	6	V	Note 1, Note 2
	FS1, FS2, FB1, FB2, ILIM1, ILIM2, SS1, SS2, LG1, LG2, REF,REG2	REG1+0.3	V	Note 1
Terminal Voltage	BOOT1, BOOT2	35	V	Note 1, Note 2
	BOOT1-SW1, BOOT2-SW2, HG1-SW1, HG2-SW2	7	V	Note 1, Note 2
	HG1	BOOT1+0.3	V	Note 1, Note 2
	HG2	BOOT2+0.3	V	Note 1, Note 2
	PGND1, PGND2	AGND±0.3	V	Note 1, Note 2
Power Dissipation1	Pd1	0.38	W	Note 3
Power Dissipation2	Pd2	0.88	W	Note 4
Power Dissipation3	Pd3	3.26	W	Note 5
Power Dissipation4	Pd4	4.56	W	Note 6
Operating Temperature Range	Topr	-20 to +100	°C	
Storage Temperature Range	Tstg	-55 to +150	°C	
Junction Temperature	Tjmax	+150	°C	

(Note 1) Not to exceed Pd.

(Note 2) Instantaneous surge voltage, back electromotive force and voltage under less than 10% duty cycle.

(Note 3) Derating in done 3.0 mW/°C for operating above Ta \geq 25°C (when don't mounted on a heat radiation board).

(Note 4) Derating in done 7.0 mW/°C for operating above Ta ≥ 25°C (Mount on 1-layer 74.2mm x 74.2mm x 1.6mm board). Surface heat dissipation copper foil:20.2mm².

(Note 5) Derating in done 26.1 mW/°C for operating above Ta ≥ 25°C (Mount on 4-layer 74.2mm x 74.2mm x 1.6mm board Two sides heat dissipation copperfoil:20.2mm². 2 or 3-layer : heat dissipation copper foil : 5505mm²).

(Note 6) Derating in done 36.5 mW/°C for operating above Ta ≥ 25°C (Mount on 4-layer 74.2mm x 74.2mm x 1.6mm board) All layers heat dissipation copper foil:5505mm².

Caution: Operating the IC over the absolute maximum ratings may damage the IC. The damage can either be a short circuit between pins or an open circuit between pins and the internal circuitry. Therefore, it is important to consider circuit protection measures, such as adding a fuse, in case the IC is operated over the absolute maximum ratings.

Recommended Operating Conditions (Ta=25°C)

Parameter	Symbol	Min	Тур	Max	Unit	Conditions
	VIN	5.5	-	28	V	
	CTL	-0.3	-	28	V	
	EN1, EN2, MCTL1, MCTL2	-0.3	-	5.5	V	
Terminal Voltage	BOOT1, BOOT2	4.5	-	33	V	
	SW1, SW2	-0.3	-	28	V	
	BOOT1-SW1, BOOT2-SW2, HG1-SW1, HG2-SW2	-0.3	-	5.5	V	
	Vo1, Vo2, PGOOD1, PGOOD2	-0.3	-	5.5	V	
Minimum ON Time	Толміл	-	-	150	nsec	
Soft Start time	Tss_max	-	-	100	ms	

This product should not be used in a radioactive environment.

Parameter	Symbol	Min	Тур	Max	Unit	Conditions
VIN Standby Current	Ізтв	70	150	250	μA	EN1= EN2= 0V, CTL= 5V
VIN Bias Current	l _{iN}	60	130	230	μA	Vo1= 5V
VIN Shut Down Mode Current	Ishd	6	12	18	μA	CTL= 0V
CTL Low Voltage	Vctll	-0.3	-	0.8	V	
CTL High Voltage	V _{CTLH}	2.3	-	28	V	
CTL Bias Current	ICTL	-18	-12	-6	μA	CTL= 0V
EN Low Voltage	V _{ENL}	-0.3	-	0.8	V	
EN High Voltage	Venh	2.3	-	5.5	V	
EN Bias Current	I _{EN}	-	3	6	μA	EN= 3V
5V Linear Regulator -VIN						
REG1 Output Voltage	V _{REG1}	4.90	5.00	5.10	V	IREG1=1mA
Maximum Current	I _{REG1}	100	-	-	mA	IREG2= 0mA, (Note 7)
Line Regulation	REG.I1	-	90	180	mV	VIN= 5.5 to 28V
Load Regulation	R _{EG.L1}	-	30	50	mV	IREG1= 0 to 30mA
3.3V Linear Regulator						
REG2 Output Voltage	V _{REG2}	3.27	3.30	3.33	V	IREG2= 1mA
Maximum Current	IREG2	100	-	-	mA	IREG1= 0mA, (Note 7)
Line Regulation	REG.I2	-	-	20	mV	VIN= 5.5 to 28V
Load Regulation	R _{EG.L2}	-	-	30	mV	IREG2= 0 to 30mA
5V Linear Regulator -Vo1						
Input Threshold Voltage	REG1th	4.1	4.4	4.7	V	Vo1: Sweep up
Input Delay Time	T _{REG1}	1.5	3.0	6.0	ms	
Switch Resistance	R _{REG1}	-	1.0	3.0	Ω	
Under Voltage Lock Out Block						
REG1 Threshold Voltage	REG1_UVLO	3.9	4.2	4.5	V	REG1: Sweep up
Hysteresis Voltage	dV_{UVLO}	50	100	200	mV	REG1: Sweep down
Output Voltage Sense Block						
Feedback Voltage1	V _{FB1}	0.693	0.700	0.707	V	
FB1 Bias Current	I _{FB1}	-	0	1	μA	FB1= REF
Output Discharge Resistance1	RDISOUT1	50	100	200	Ω	
Feedback Voltage2	V _{FB2}	0.693	0.700	0.707	V	
FB2 Bias Current	I _{FB2}	-	0	1	μA	FB2= REF
Output Discharge Resistance2	R _{DISOUT2}	50	100	200	Ω	
H ³ REG [™] Control Block						
On Time1	ton1	0.760	0.910	1.060	μs	Vo1= 5V,FS1= 51kΩ
On Time2	ton2	0.470	0.620	0.770	μs	Vo2= $3.3V$,FS2= $51k\Omega$
Maximum On Time 1	tonmax1	2.5	5	10	μs	Vo1= 5V
Maximum On Time 2	t _{ONMAX} 2	1.65	3.3	6.6	μs	Vo2= 3.3V
Minimum Off Time	toffmin	-	0.2	0.4	μs	
FET Driver Block						
HG High Side ON Resistance	HGHON	-	3.0	6.0	Ω	
HG Low Side ON Resistance	HGLON	-	2.0	4.0	Ω	
LG High Side ON Resistance	LGHON	-	2.0	4.0	Ω	
LG Low Side ON Resistance	LGLON	-	0.5	1.0	Ω	

(Note 7) $I_{REG1}+I_{REG2} \leq 100 \text{mA}$.

Electrical Characteristics (Unless otherwise noted, Ta=25°CVIN=12V, CTL=OPEN, EN1=EN2=5V, FS1=FS2=51kΩ)

Over Voltage Protection Block						
OVP Threshold Voltage	Vovp	0.77 (+10%)	0.84 (+20%)	0.91 (+30%)	V	
OVP Hysteresis	dV_ovp	50	150	300	mV	
Output Short Protection Block						
SCP Threshold Voltage	VSCP	0.42 (-40%)	0.49 (-30%)	0.56 (-20%)	V	
Delay Time	TSCP	0.4	0.75	1.5	ms	
Over Current Protection Block						
Offset Voltage	dVsmax	80	100	120	mV	ILIM= 100kΩ
Power Good Block						
Power Good Low Threshold	Vpgthl	0.525 (-25%)	0.595 (-15%)	0.665 (-5%)	V	
Power Good Low Voltage	Vpgl	-	0.1	0.2	V	IPGOOD= 1mA
Delay Time	TPGOOD	0.4	0.75	1.5	ms	
Power Good Leakage Current	ILEAKPG	-2	0	2	μA	VPGOOD= 5V
Soft Start Block						
Charge Current	Iss	1.5	2.3	3.1	μA	
Standby Voltage	VSS_STB	-	-	50	mV	
Mode Control Block				·		
MCTL Low Voltage	VMCTL_L	-0.3	-	0.3	V	
MCTL High Voltage	VMCTL_H	2.3	-	REG1 +0.3	V	
MCTL Bias Current	IMCTL	8	16	24	μA	MCTL= 5V

Typical Performance Curves (Reference data)

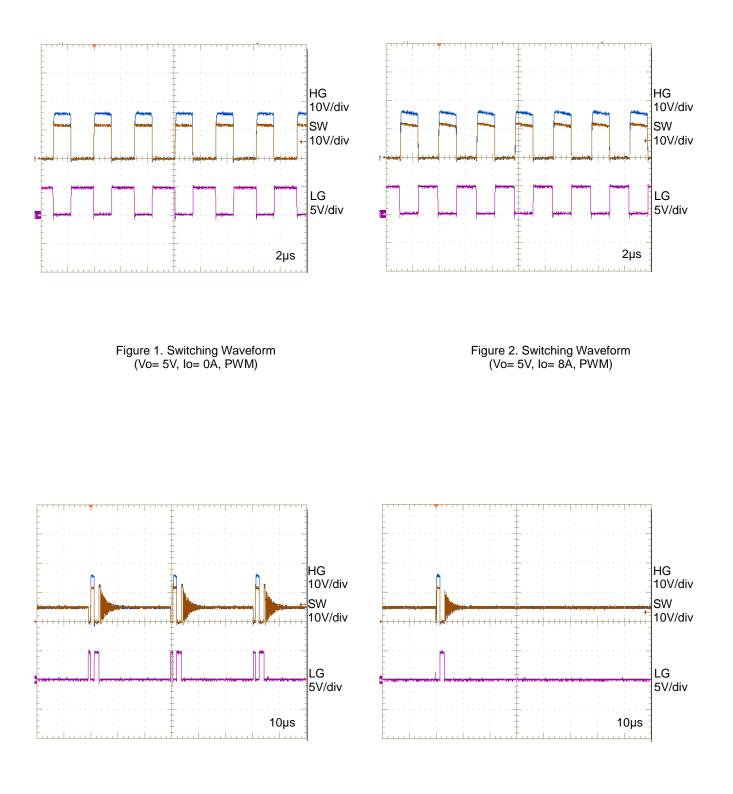


Figure 3. Switching Waveform (Vo= 5V, Io= 0A, QLLM) Figure 4. Switching Waveform (Vo= 5V, Io= 0A, SLLM)

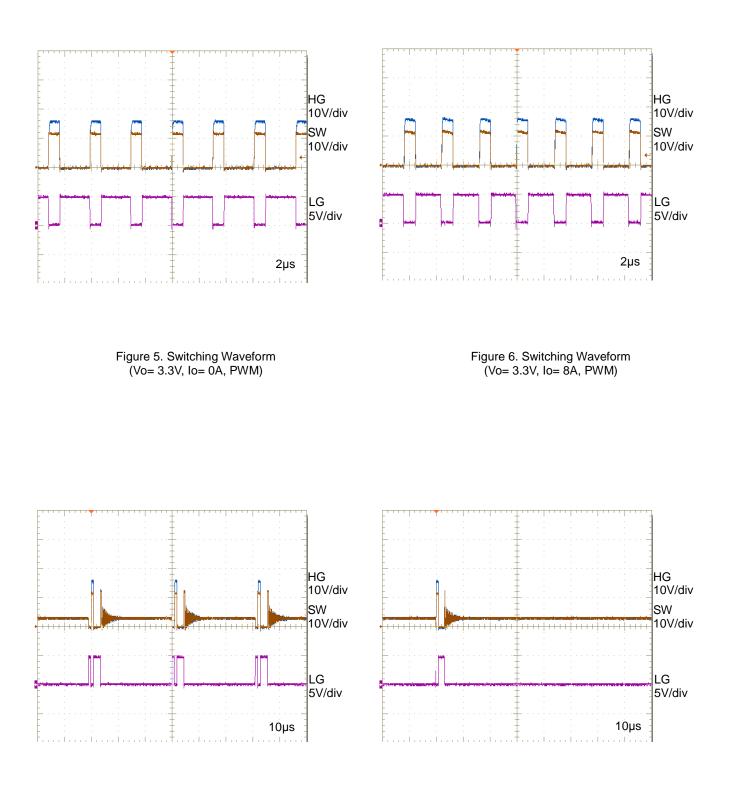


Figure 7. Switching Waveform (Vo= 3.3V, Io= 0A, QLLM) Figure 8. Switching Waveform (Vo= 3.3V, Io= 0A, SLLM)

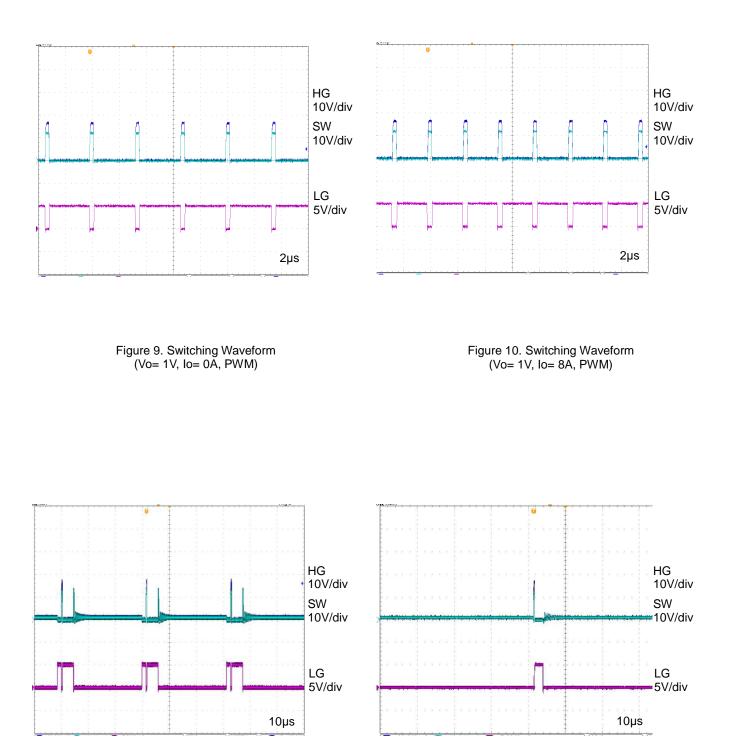
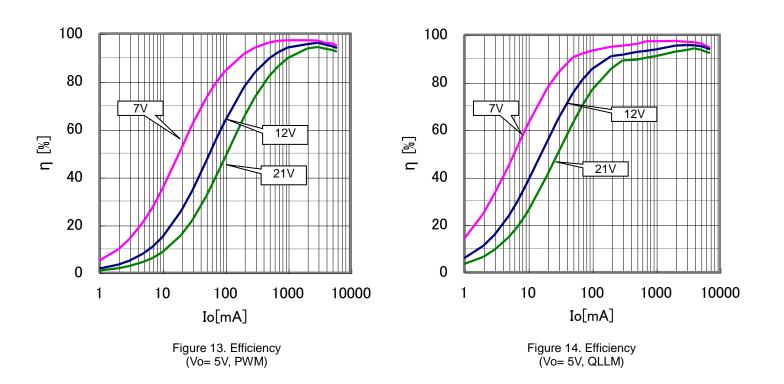
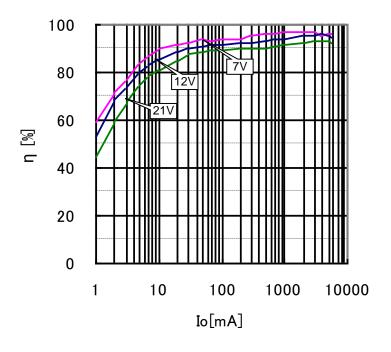
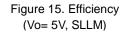


Figure 11. Switching Waveform (Vo= 1V, Io= 0A, QLLM)

Figure 12. Switching Waveform (Vo= 1V, Io= 0A, SLLM)







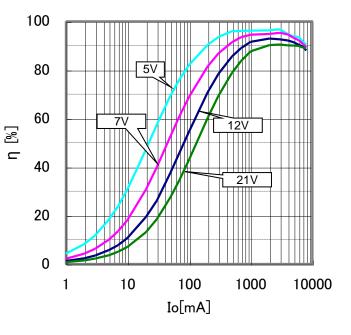


Figure 16. Efficiency (Vo= 3.3V, PWM)

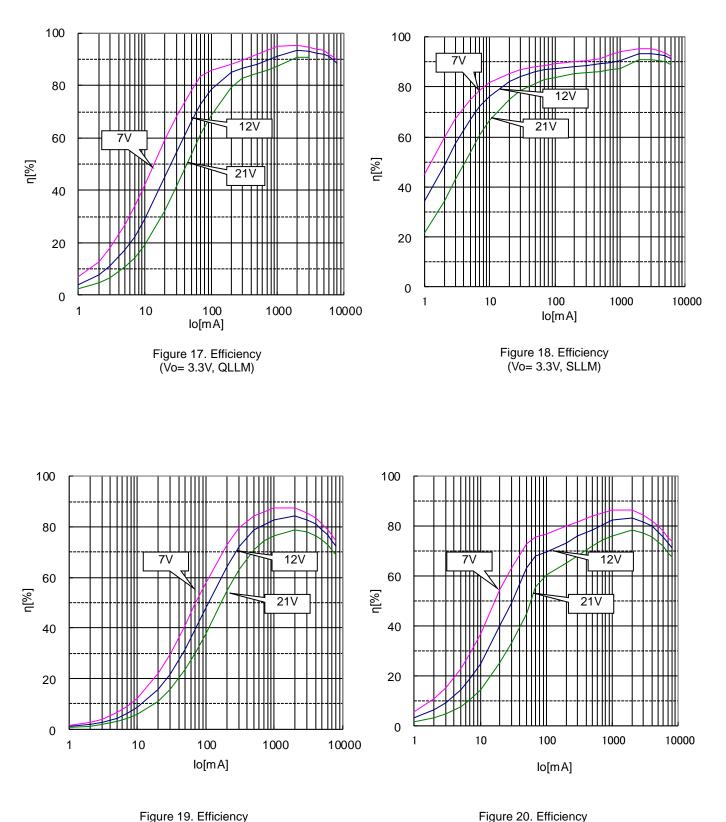
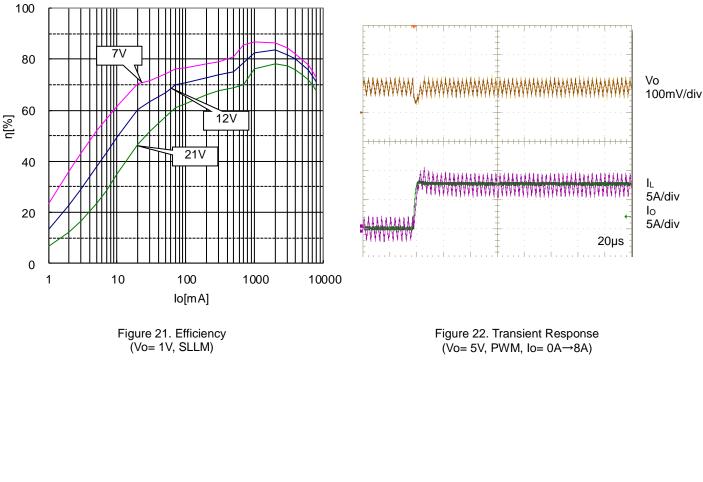


Figure 20. Efficiency (Vo= 1V, QLLM)

(Vo= 1V, PWM)



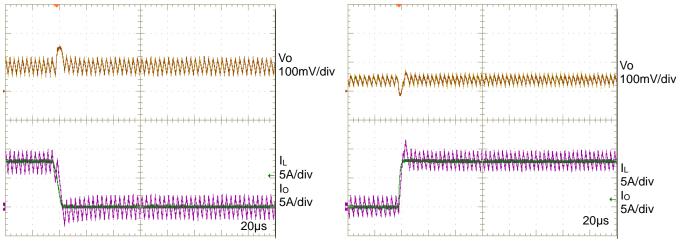


Figure 23. Transient Response (Vo= 5V, PWM, Io= 8A→0A) Figure 24. Transient Response (Vo= 3.3V, PWM, Io= 0A→8A)

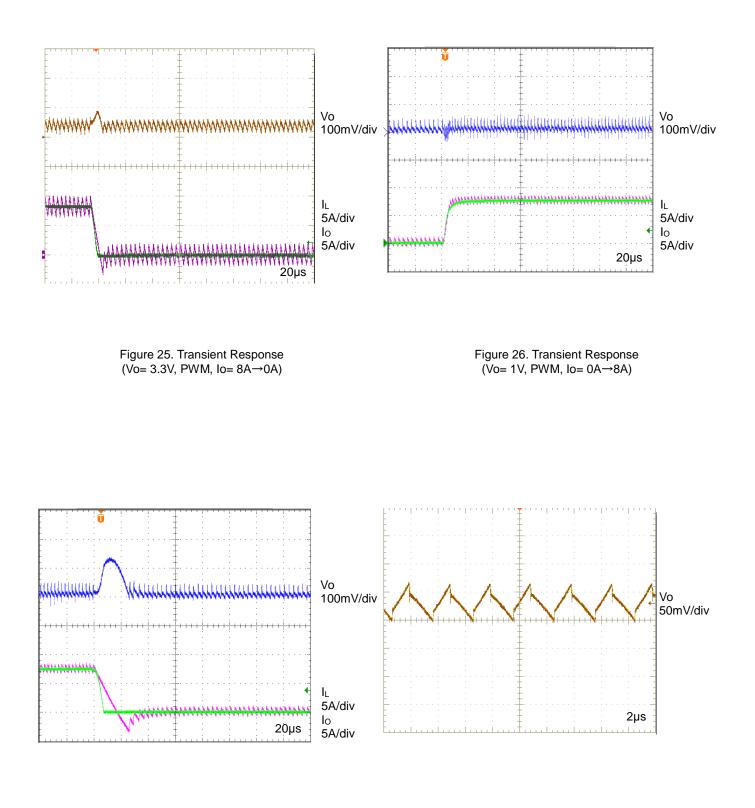


Figure 27. Transient Response (Vo= 1V, PWM, Io= 8A→0A)

Figure 28. Output Voltage (Vo= 5V, PWM, Io= 0A)

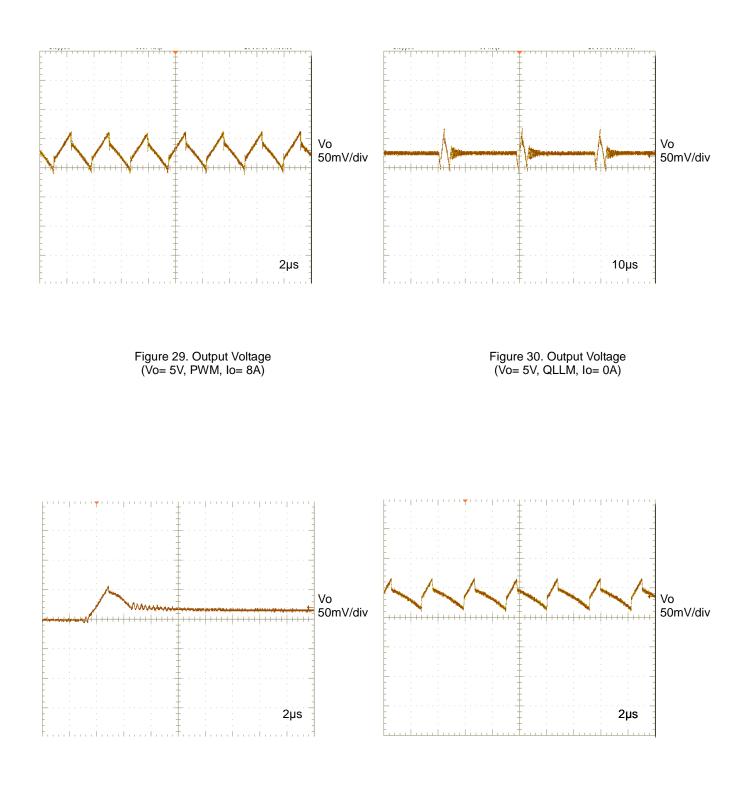


Figure 31. Output Voltage (Vo= 5V, SLLM, Io= 0A)

Figure 32. Output Voltage (Vo= 3.3V, PWM, Io= 0A)

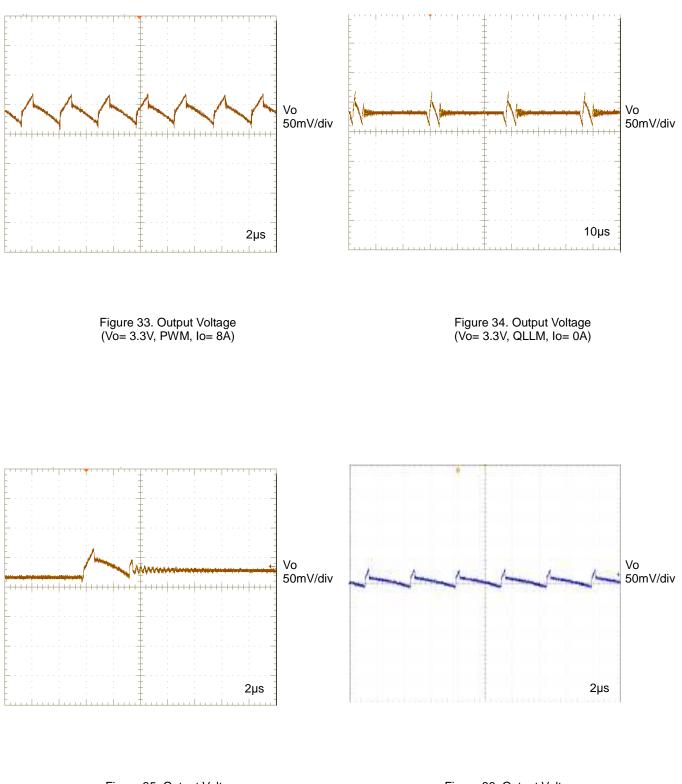
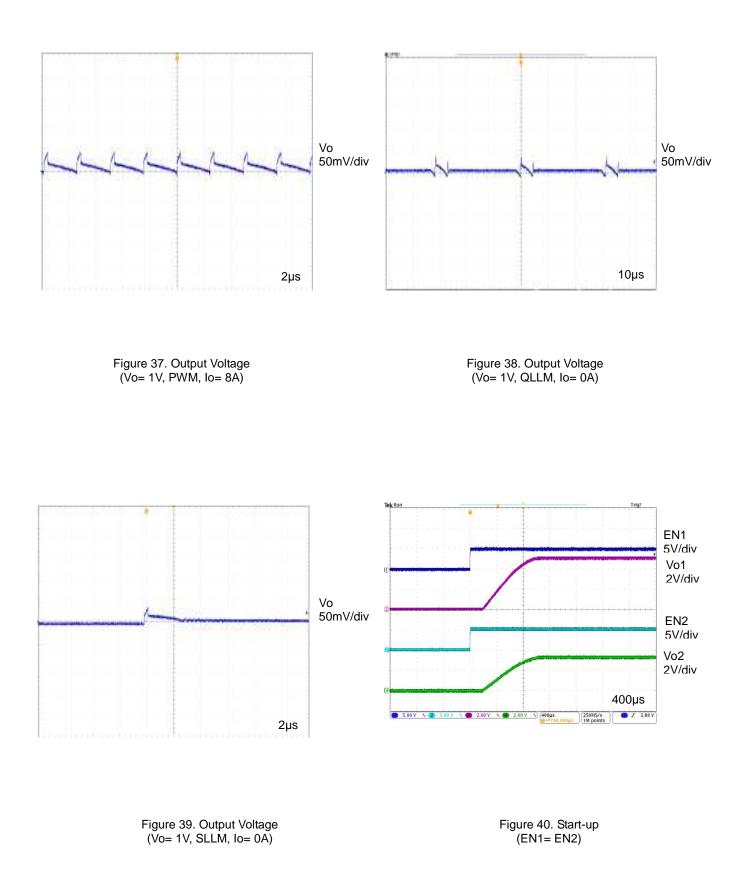


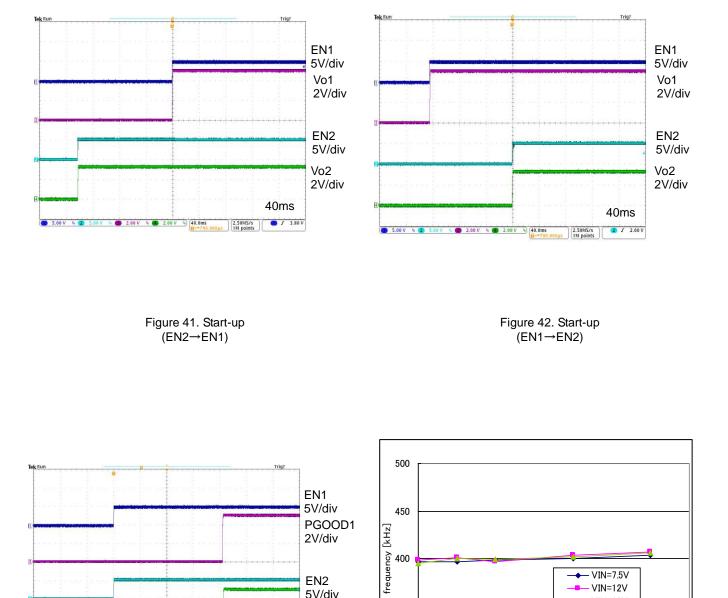
Figure 35. Output Voltage (Vo= 3.3V, SLLM, Io= 0A)

Figure 36. Output Voltage (Vo= 1V, PWM, Io= 0A)



● 5.00 V ½ ② 5.00 V ≤ ● 2.00 V ½ ● 2.00 V ½ ▲ 100µs #→706.000µs

Typical Performance Curves - continued



EN2

40ms

2 J 2.60 V

5V/div

PGOOD2 2V/div

350

300

0

1

2

Figure 43. Start-up (EN1/2→PGOOD1/2)

Figure 44. Io-frequency $(Vo=5V, PWM, RFS=68k\Omega)$

3

IOUT [A]

4

VIN=7.5V

VIN=12V

VIN=18V

5

6

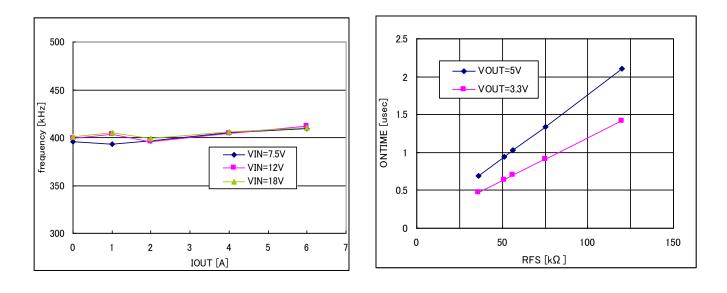
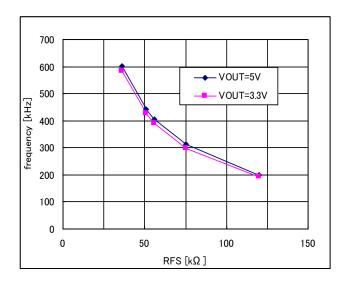


Figure 45. lo-frequency (Vo= 3.3V, PWM, RFS= $68k\Omega$)

Figure 46. On time-RFS



5.500 5.000 4.500 VIN=7.5V(-5°C) . - VIN=21V(-5°C) 4.000 . - VIN=7.5V(75°C) 3.500 - VIN=21V(75°C) Σ 3.000 VOUT 2.500 2.000 1.500 1.000 0.500 0.000 0 2 4 6 8 10 12 14 16 IOUT [A]

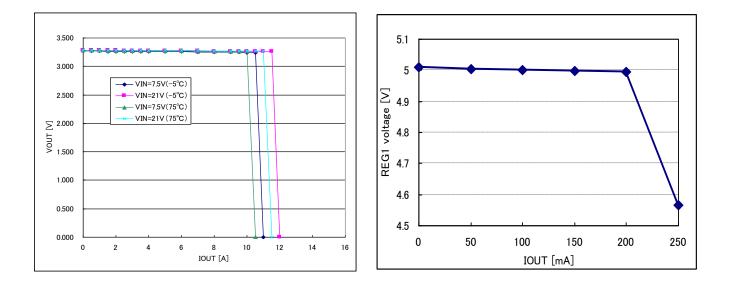


Figure 49. Current Limit (Vo= 3.3V)

Figure 50. REG1 Load Regulation

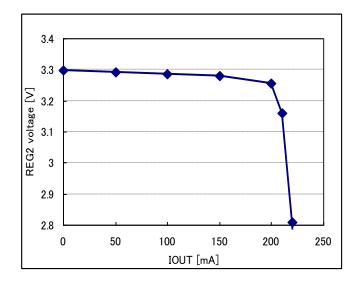
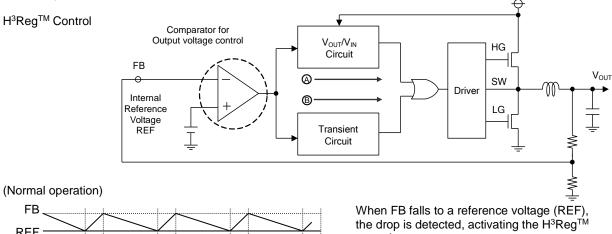


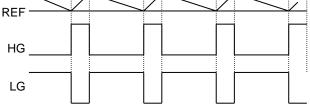
Figure 51. REG2 Load Regulation

Description of Block

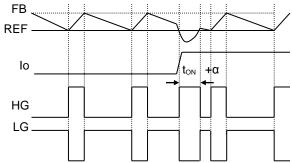
BD9528AMUV is a dual channel synchronous buck regulator using H³Reg[™], Rohm's latest constant on-time controller technology. Fast load response is achieved by controlling the output voltage using a comparator without relying on the switching frequency.

When VOUT drops due to a rapid load change, the system quickly restores VOUT by extending the ton time interval. Thus, it serves to improve the regulator's transient response. Activation of the light load mode further increases efficiency by using VIN Simple Light Load Mode (SLLM) control.





(VOUT drops due to a rapid load change)



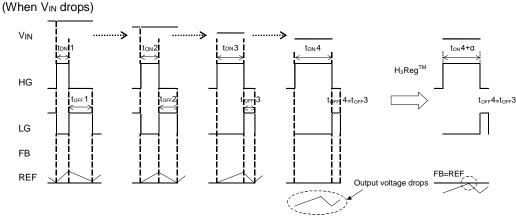
control system

$$t_{ON} = \frac{V_{OUT}}{V_{IN}} \times \frac{1}{f} [sec] \cdot \cdot \cdot (1)$$

HG output on-time is determined by the formula (1). When HG is off, LG is on until the output voltage becomes FB= REF.

After the status of HG is off, LG go on outputting until output voltage become FB= REF.

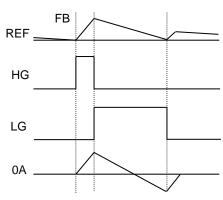
When VOUT drops due to a rapid load change, and the voltage remains below the output setting following the programmed ton time, the system quickly restores Vout by extending the ton time, thus improving the transient response. Once VOUT is restored, the controller continues normal operation.



Based on the value of VIN, the on-time ton and off-time toFF are determined by toN= Vout / VIN x I/f and toFF= (VIN- VOUT)/VIN. As the V_{IN} voltage drops, in order to maintain the output voltage, ton becomes longer and toFF is shorter. However, for normal operation, if V_{IN} drops further, t_{ON} is longer and t_{OFF} tminoff (minimum off- time is defined internally), the output voltage will decrease because toFF cannot be any shorter than the minimum off-time. With H³RegTM, if V_{IN} goes even lower, the output voltage is maintained as the ton time is extended. (ton time is extended until FB>REF). In this case, the switching frequency is lowered so that the ton time can be extended.

Description of Block - continued

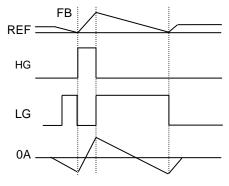
Light Load Control (SLLM)



SLLM will activate when the LG pin is off and the coil current is near 0A (current flows from V_{OUT} to SW).

When the FB input is lower than the REF voltage again, HG will be enabled once again.

(QLLM)

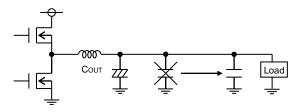


QLLM will activate when the LG pin is off and the coil current is near 0A (current flows from V_{OUT} to SW). In this case, the next HG is prevented. Then, when FB falls below the output programmed voltage within the programmed time (Typ= 40µs), HG will resume. In the case where FB doesn't fall in the programmed time, LG is forced on causing V_{OUT} to fall. As a result, the next HG is on.

MCTL1	MCTL2	Control Mode	Start-up
L	L	SLLM	PWM
L	Н	QLLM	PWM
Н	Х	PWM	PWM

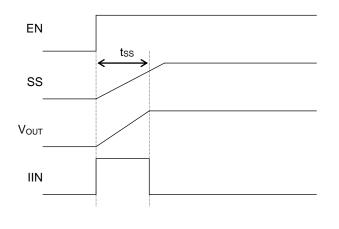
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*Attention: To effect the rapid transient response, the H³Reg[™] control monitors the current from the output capacitor to the load using the ESR of the output capacitor Do not use ceramic capacitors on C_{OUT} side of power supply. Ceramic bypass capacitors can be used near the individual loads if desired. The BD9528AMUV operates in PWM mode until the SS input reaches the clamp voltage (2.5V), regardless of the control mode setting, this assures stable operation while the during soft start.



Timing Chart

Soft Start Function



Soft start is exercised with the EN pin set high. Current control takes effect at startup, enabling a moderate output voltage "ramping start." Soft start timing and incoming current are calculated with formulas (2) and (3) below.

Soft start time

tss =
$$\frac{0.7(\text{Typ}) \times \text{Css}}{2.3\mu\text{A}(\text{Typ})} < 100\text{m} \text{ [sec]} \cdot \cdot \cdot (2)$$

C _{SS} (pF)	Soft start time(ms)
18000	5
33000	10
68000	20

Inrush current

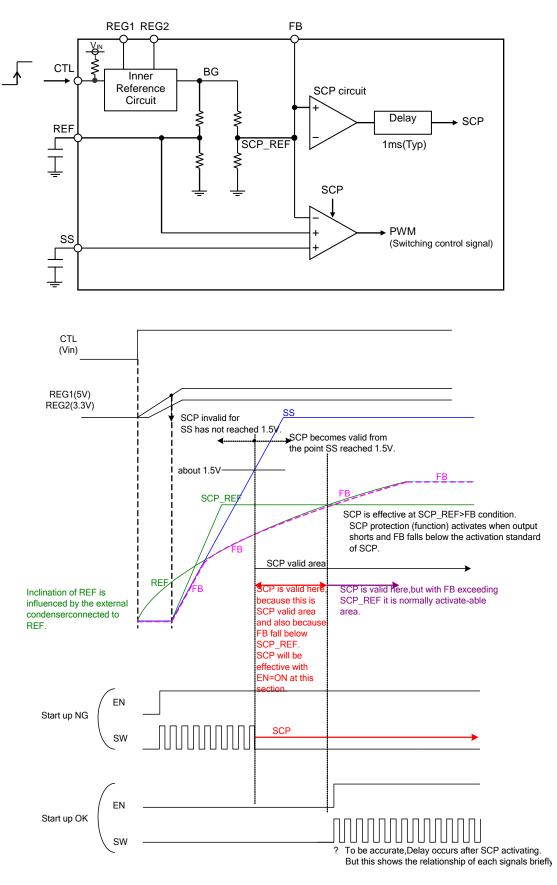
$$Iin = \frac{Co \times V_{OUT}}{tss} \times \frac{V_{OUT}}{V_{IN}} [A] \cdot \cdot \cdot (3)$$

(Css: Soft start capacitor Co: Output capacitor)

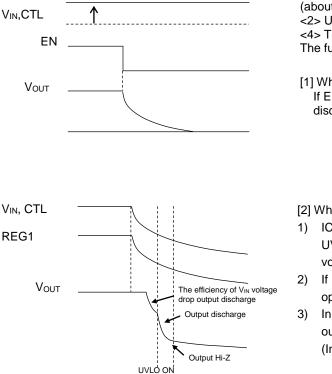
*Notice : Max ontime function is disable by SS voltage reach to 2.5V.

Timing Chart - continued

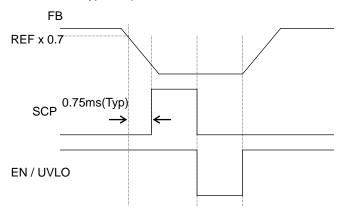
- · Notes when waking up with CTL pin or VIN pin
 - If EN pin is high or short (or pull up resistor) to REG1 pin, IC starts up by switching CTL pin, the IC might fail to start up (SCP function) with the reason below, please be careful of SS pin and REF pin capacitor capacity.



Output Discharge



Timer Latch Type Output Short Circuit Protection



It will be available to use if connecting V_{OUT} pin to DC/DC output. (about 100 Ω). Discharge function operates when <1> EN='L' <2> UVLO= ON(If input voltage is low) <3> SCP latch <4> TSD= ON.

The function at output discharge time is shown as left.

 When switch to low from high with EN pin.
 If EN pin voltage is below than EN threshold voltage, output discharge function is operated, and discharge output capacitor charge.

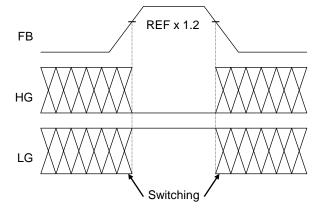
[2] When switch to low from high with EN pin

- IC is in normal operation until REG1 voltage becomes lower than UVLO voltage. However, because V_{IN} voltage also becomes low, output voltage will drop, too.
- If REG1 voltage reaches the UVLO voltage, output discharge function is operated, and discharge output capacitor charge.
- B) In addition, if REG1 voltage drops, inner IC logic cannot operate, so that output discharge function does not work, and becomes output Hi-z. (In case, FB has resistor against ground, discharge at the resistor.)

Short protection is enabled when the output voltage falls to or below REF X 0.7.

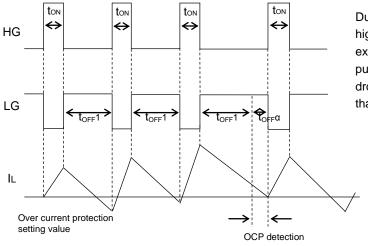
Once the programmed time period has elapsed, the output is latched off to prevent destruction of the circuit. (HG= Low, LG= Low) Output voltage can be restored either by cycling the EN pin or disabling UVLO.

Over Voltage Protection



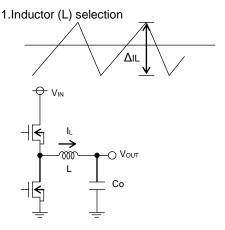
When the output voltage increases to or above REF x 1.2(Typ), output over voltage protection is enabled, and the Low-side FET turns on to reduce the output. (LG= High, HG= Low). When the output falls to within normal operation, the function is restored to normal operation.

www.rohm.co.jp © 2015 ROHM Co., Ltd. All rights reserved. TSZ22111 • 15 • 001 Over current protection circuit



During normal operation, if FB is less than REF, HG is high during the time t_{ON} , but when the coil current exceeds the I_{LIMIT} threshold, HG is set to off. The next pulse returns to normal operation if the output voltage drops after the maximum on-time or I_L becomes lower than I_{LIMIT} .

Selection of Components Externally Connected



Output ripple current

The inductor value is a major influence on the output ripple current. As formula (4) below indicates, the greater the inductor or the switching frequency, the lower the ripple current.

$$\Delta I_{L=} \frac{(V_{IIN}-V_{OUT}) \times V_{OUT}}{L \times V_{IN} \times f} [A] \cdot \cdot \cdot (4)$$

Generally, lower inductance values offer faster response times but also result in increased output ripple and lower efficiency.

0.47µH to 2.2µH are recommended as appropriate setting value.

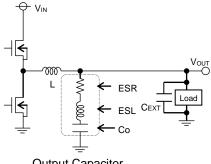
The peak current rating of coil is approximated by formula (5). Please select inductor which is higher than this value.

$$|_{\text{LPEAK}= \text{IOUTMAX} + \frac{(V_{\text{IN}} - V_{\text{OUT}}) \times V_{\text{OUT}}}{2 \times L \times V_{\text{IN}} \times f} [A] \cdot \cdot \cdot (5)$$

*Passing a current larger than inductor's rated current will cause magnetic saturation in the inductor and decrease system efficiency. In selecting the inductor, be sure to allow enough margin to assure that peak current does not exceed the inductor rated current value.

*To minimize possible inductor damage and maximize efficiency, choose an inductor with a low (DCR, ACR) resistance.

2. Output Capacitor (Co) Selection



The output capacitor should be determined by equivalent series resistance and equivalent series inductance so that the output ripple voltage is 30mV or more.

The rating of the capacitor is selected with sufficient margin given the output voltage.

 $\Delta V_{OUT} = \Delta IL \times ESR + ESL \times \Delta IL / t_{ON} \cdot \cdot \cdot (6)$

ΔIL: Output ripple current ESR: Equivalent series resistance, ESL: Equivalent series inductance

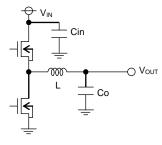
Output Capacitor

Please give due consideration to the conditions in formula (7) below for the output capacitor, bearing in mind that the output start-up time must be established within the soft start timeframe. Capacitors used as bypass capacitors are connected to the load side affect the overall output capacitance (C_{EXT}, figure above). Please set the soft start time or over-current detection value, regarding these capacities.

$$Co+C_{EXT} \leq \frac{T_{SS} x \text{ (Limit- I_{OUT})}}{V_{OUT}} \cdot \cdot \cdot (7) \qquad T_{SS} : Soft start time \\ Limit : Over current detection$$

Note: If an inappropriate capacitor is used, OCP may be detected during activation and may cause startup malfunctions.

3. Input Capacitor (Cin) Selection



The input capacitor selected must have low enough ESR to fully support high output ripple so as to prevent extreme over current conditions. The formula for ripple current IRMS is given in (8) below.

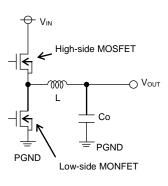
$$RMS = I_{OUT} \times \frac{\sqrt{V_{OUT} (V_{IN} - V_{OUT})}}{V_{IN}} \quad [A] \cdot \cdot \cdot (8)$$

Where VIN= 2 x VOUT, IRMS= $\frac{I_{OUT}}{2}$

Input Capacitor

A ceramic capacitor is recommended to reduce ESR loss and maximize efficiency.

4.MOSFET Selection



High-side driver and Low-side driver are designed to activate N channel MOSFET's with low on-resistance.

The chosen MOSFET may result in the loss described below, please select a proper FET for each considering the input-output and load current.

< Loss of High-side MOSFET >

Pmain= PRON+PTRAN

$$= \frac{V_{OUT}}{V_{IN}} x \operatorname{Ron} x \operatorname{Iout}^2 + \frac{(\operatorname{Tr}+\operatorname{Tf}) x V_{IN} x \operatorname{Iout} x f}{6} \cdot \cdot \cdot (9)$$

(Ron: On-resistance of FET f: Switching frequency Tr: Rise time, Tf: Fall time)

< Loss of Low-side MOSFET >

Psyn= PRON

$$= \frac{V_{\text{IN}} - V_{\text{OUT}}}{V_{\text{IN}}} x \text{ Ron } x \text{ I}_{\text{OUT}}^2 \cdots (10)$$

The High-side MOSFET generates loss when switching, along with the loss due to on-resistance. Good efficiency is achieved by selecting a MOSFET with low on-resistance and low Qg (gate total charge amount). Recommended MOSFETs for various current values are as follows:

Output current	High-side MOSFET	Low-side MOSFET					
to 5A	RQ3E080GN	RQ3E100GN					
5 to 8A	RQ3E120GN	RQ3E150GN					
8 to 10A	RQ3E150GN	RQ3E180GN					

5. Output Voltage Set Point

This IC operates such that output voltage is REF ≅ FB.

<Output Voltage>

 $V_{OUT} = \frac{(R1+R2)}{R2} \times REF(0.7V) + \frac{1}{2} \Delta V_{OUT} \qquad (\Delta V_{OUT}: Output ripple voltage)$ $\Delta V_{OUT} = \Delta I_L \times ESR \qquad (\Delta I_L: ripple current of coil)$ $\Delta I_L = (V_{IN} - V_{OUT}) \times \frac{V_{OUT}}{(L \times V_{IN} \times f)} \qquad L: inductance[H] f: switching frequency[Hz]$

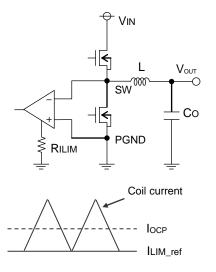
*(Notice)Please set output ripple voltage more than 30mV to 50mV.

(Example) V_{IN} = 20V, V_{OUT} = 5V, f= 300kHz, L= 2.5µH, ESR= 20mΩ, R1= 56kΩ, R2= 9.1kΩ

$$\Delta I_L = (20V-5V) \times \frac{5V}{(2.5 \times 10^{-6}H \times 20V \times 300 \times 10^{3}Hz)} = 5(A)$$

 $\Delta V_{OUT} = 5A \times 20 \times 10^{-3}\Omega = 0.1(V)$
 $V_{OUT} = 0.7V \times \frac{(51k\Omega + 9.1k\Omega)}{9.1k\Omega} + \frac{1}{2} \times 0.1V = 5.057(V)$
 V_{IN}
REF $O_{II} = O_{II} = O_{$

6. Setting over current protection



The on resistance (between SW and PGND) of the low side MOSFET is used to set the over current protection.

Over current reference voltage (I_{LIM_ref}) is determined as in formula(11) below.

$$I_{\text{LIM_ref}} = \frac{10k}{\text{R}_{\text{ILIM}}[k\Omega] \times \text{R}_{\text{ON}}[m\Omega]} [A] \cdot \cdot \cdot (11)$$

 $(R_{ILIM}$: Resistance for setting of over current voltage protection value[k Ω] R_{ON}: Low-side on resistance value of FET[m Ω])

Over current protection is actually determined by the formula (12) below.

$$= I_{\text{LIM_ref}} + \frac{1}{2} X \frac{V_{\text{IN}} - V_{\text{O}}}{L} X \frac{I}{f} X \frac{V_{\text{O}}}{V_{\text{IN}}} \cdot \cdot \cdot (12)$$

ΔIL:Coil ripple current[A] V_{IN}:Input voltage[V] V₀:Output voltage [V] f:Switching frequency [H₂] L:Inductance [H]

(Example)

I

If a load current 5A is desired with V_{IN}=6 to 19V, V_{OUT}=5V, f=400kHZ, L=2.5µH, RON=20mΩ, the formula would be:

$$OCP = \frac{10k}{\text{RILIM}[k\Omega] \times \text{RON}[m\Omega]} + \frac{1}{2} \times \frac{\text{V}_{\text{IN}} - \text{V}_{\text{O}}}{\text{L}} \times \frac{1}{\text{f}} \times \frac{\text{V}_{\text{O}}}{\text{V}_{\text{IN}}} > 5$$

When V_{IN} = 6V, I_{OCP} will be minimum(this is because the ripple current is also minimum) so that if each condition is input, the formula will be the following: RILIM<109.1[k Ω].

*To design the actual board, please consider enough margin for FET on resistance variation, Inductance variation, IC over current reference value variation, and frequency variation.

7. Relation between output voltage and t_{ON} time

For BD9528AMUV, both channels, are high efficiency synchronous regulator controllers with variable frequency. t_{ON} time varies with Input voltage [V_{IN}], output voltage [V_{OUT}], and RFS of FS pin resistance.

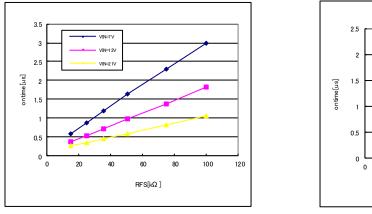


Figure55. RFS - ontime(V_{OUT}= 5V)

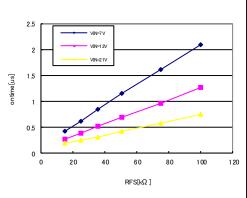


Figure 56. RFS – ontime(V_{OUT}= 3.3V)

From ton time, frequency on application condition is following:

Frequency =
$$\frac{V_{OUT}}{V_{IN}} \times \frac{1}{t_{ON}} [kHz] \cdot \cdot \cdot (13)$$

However, real-life considerations (such as the external MOSFET gate capacitor and switching speed) must be factored in as they affect the overall switching rise and fall time, so please confirm by experiment.

Application Example (Vin= 12V, Vo1= 3.3V/8A, f1= 400kHz, Vo2= 2.5V/8A, f2= 400kHz)

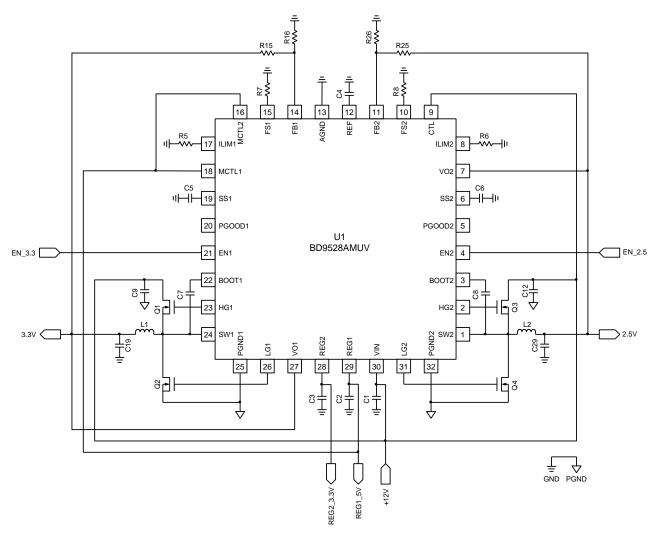
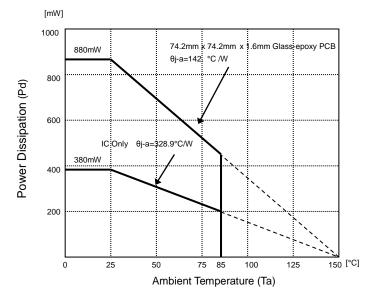


Figure 57. Application Example

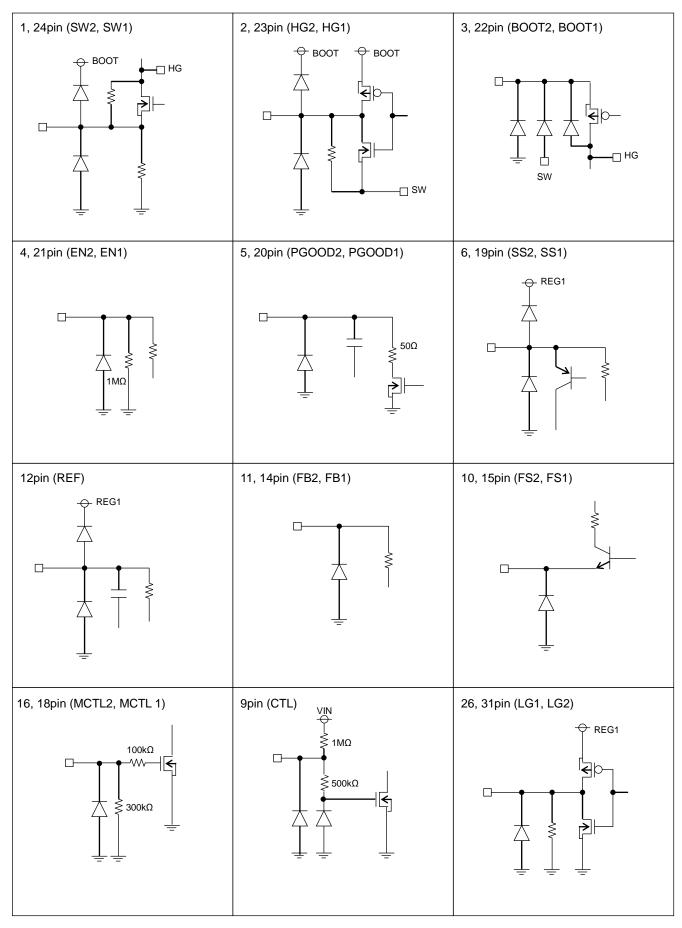
Reference Designator	Туре	Value	Description	Manufacturer Part Number	Manufacturer	Configuration (mm)
C1, C9, C10, C11, C12	Ceramic Capacitor	10µF	35V, X5R, ±10%	GRM32ER6YA106KA12	MURATA	3225
C2, C3	Ceramic Capacitor	10µF	16V, X5R, ±10%	GRM21BR61C106ME15	MURATA	2012
C4, C5, C6	Ceramic Capacitor	0.1µF	16V, X5R, ±10%	GRM155R61C104KA88	MURATA	1005
C7, C8	Ceramic Capacitor	0.47µF	10V, X5R, ±10%	GRM188R61A474KA61	MURATA	1608
C18, C19, C28, C29	POSCAP	330µF	6.3V, ±20%, ESR 18mΩmax	6TPE330MIL	SANYO	7343
L1,L2	Inductor	1µH	±20%,10A(L=-30%), DCR=5.8mΩ±10%	GLMC1R003A	ALPS	6565
Q1, Q3	MOSFET	-	N-ch, Vdss 30V, Id 15A, Ron 4.7mΩ	RQ3E150GN	ROHM	3333
Q2, Q4	MOSFET	-	N-ch, Vdss 30V, Id 18A, Ron 3.3mΩ	RQ3E180GN	ROHM	3333
R5, R6	Resistor	62kΩ	1/16W, 50V, 5%	MCR01MZPJ623	ROHM	1005
R7, R8	Resistor	51kΩ	1/16W, 50V, 5%	MCR01MZPJ513	ROHM	1005
R15	Resistor	16kΩ	1/16W, 50V, 0.5%	MCR01MZPD1602	ROHM	1005
R16	Resistor	4.3kΩ	1/16W, 50V, 0.5%	MCR01MZPD4301	ROHM	1005
R24	Resistor	100Ω	1/16W, 50V, 5%	MCR01MZPJ101	ROHM	1005
R25	Resistor	12kΩ	1/16W, 50V, 0.5%	MCR01MZPD1202	ROHM	1005
R26	Resistor	4.7kΩ	1/16W, 50V, 0.5%	MCR01MZPD4701	ROHM	1005
U1	IC	-	Buck DC/DC Controller	BD9528AMUV	ROHM	VQFN032V5050

Without any ripple (about 10mV), there is a possibility that the FB signal is not stable due to the adoption of the comparator control method. Please ensure enough ripple voltage either by (1)reducing the L-value of inductor, or (2)using high ESR output capacitor. Ripple voltage can be generated in FB terminal by adding a capacitor in parallel to resistor (R17, R19) of the FB input, but the circuit will be sensitive to noise from the output (Vo1/Vo2) line and is not recommended. Stability of the circuit is influenced by the layout of the PCB, please pay careful attention to the layout.

Power Dissipation

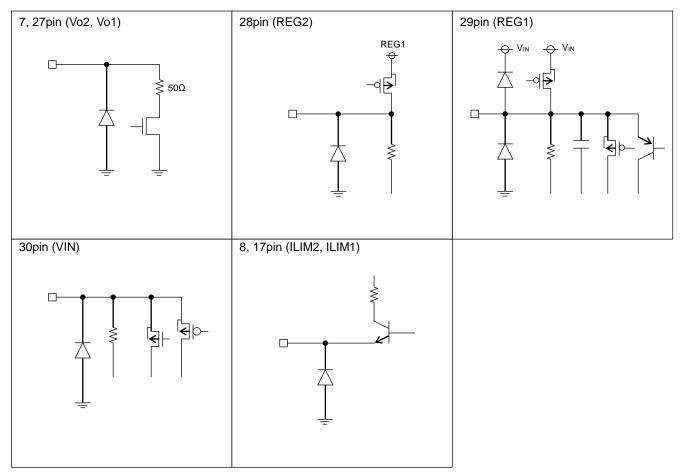


I/O equivalence circuits

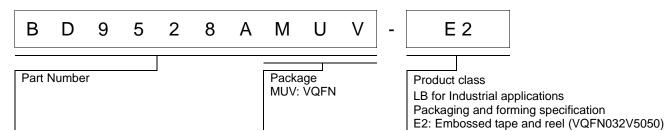


BD9528AMUV

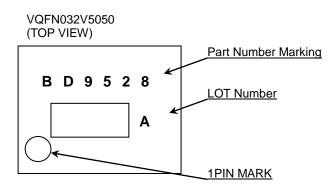
I/O equivalence circuit(s) - continued

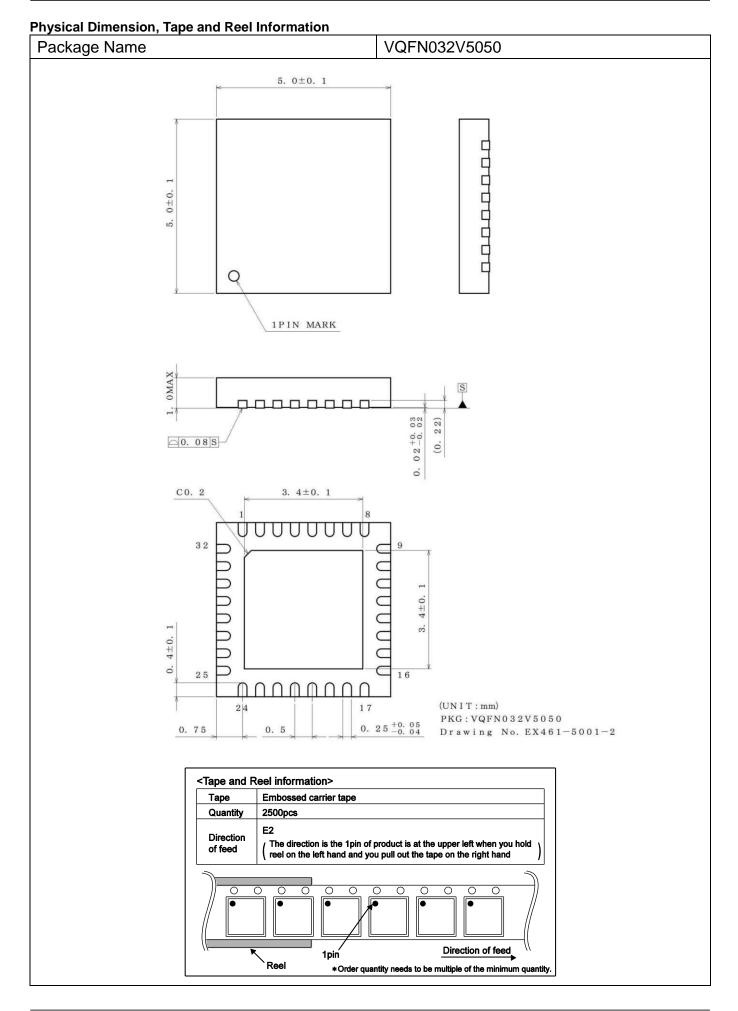


Ordering Information



Marking Diagrams





Revision History

Date	Revision	Changes
8.Jul.2016	001	New Release(Change Format)

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(Note1) Medical Equipment Classification of the Specific	Applications
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JAPAN	USA	EU	CHINA
CLASSⅢ	CLASSI	CLASS II b	CLASSII
CLASSⅣ		CLASSⅢ	

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 - [f] Sealing or coating our Products with resin or other coating materials
 - [g] Use of our Products without cleaning residue of flux (even if you use no-clean type fluxes, cleaning residue of flux is recommended); or Washing our Products by using water or water-soluble cleaning agents for cleaning residue after soldering
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